

# AQUIFER PROTECTION DISTRICT - HYDROGEOLOGIC STUDY REPORT TUCK REALTY CORPORATION, PROPOSED CONDOMINIUM DEVELOPMENT MAP 10, LOT 1 LAFAYETTE ROAD RYE, NEW HAMPSHIRE

Prepared for:

Tuck Realty Corporation P.O. Box 190 Exeter, New Hampshire 03833

Prepared By:

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June 17, 2021

PROJECT 9212-007 | June 17, 2021 NEW HAMPSHIRE | MASSACHUSETTS | CONNECTICUT | MAINE GEOINSIGHT.COM | INFO@GEOINSIGHT.COM | 800.271.1953



June 17, 2021

GeoInsight Project 9212-007

Kimberly Reed Town of Rye Planning & Zoning Administrator 10 Central Road Rye, New Hampshire 03870

RE: Aquifer Protection District – Hydrogeologic Study Report Tuck Realty Corporation, Proposed Condominium Development Map 10, Lot 1, Lafayette Road Rye, New Hampshire

Dear Ms Reed:

At the request of Tuck Realty Corporation (Tuck), GeoInsight, Inc. (GeoInsight) completed a Hydrogeologic Study of a vacant parcel of land adjacent to Lafayette Road (Route 1) in Rye, New Hampshire (the Property). The Property is identified by the Town of Rye as Map 10, Lot 1 and is a 9.56-acre parcel that was formerly known as 355 Lafayette Road (former Hector's Motel). The location of the Property is shown on Figure 1 and on the Rye Assessors map included in Attachment A. The Hydrogeologic Study was completed pursuant to Town of Rye General Code, §190-3.6 E(2) and F(1). Based upon the mapped limits of stratified-drift aquifers (June 2003 Town map in Attachment A), and according to Rye General Code, §190-3.6, the Property is located within the Town's Aquifer and Wellhead Protection Overlay District.

As you may be aware, a lot line revision is proposed which would separate the Property into two new parcels. Redevelopment efforts include the construction of a proposed 30-unit condominium (condo) development on the southern portion of the parcel by Tuck and construction of a senior living facility by Benchmark Senior Living (Benchmark) on the northern portion of Map 10, Lot 1, with future connection of the senior facility to Benchmark's Evolve Memory Care (Evolve) facility, located on the abutting parcel farther to the north. Current preliminary layouts of the Tuck condo development and proposed Benchmark assisted living facility are presented on Figures 2 and 3.

This Hydrogeologic Study Report addresses the Tuck condo development as it relates to the Town's Aquifer Protection District rules and requirements with a separate Hydrogeologic Study Report anticipated to be submitted under separate cover for Benchmark's proposed facility on the future northern portion of the subdivided lot. Soil boring and monitoring well data from the entire current parcel, and existing data from wells at the Evolve facility were considered in development of this Hydrogeologic Study.

# PROPOSED DEVELOPMENT DETAILS

Tuck has proposed 10 residential condo buildings each comprised of three, 2-bedroom condo units. Each building will be served by on-site subsurface disposal systems ("leach fields"), 10 total,

with design flows of 320 gallons per day (GPD) per unit, or 960 GPD per field. GeoInsight understands stormwater will be managed in the development using porous pavement and sheet flow to vegetated/landscaped areas and roof line drip edges to minimize and manage runoff. A stormwater retention or infiltration basin to collect and manage collected stormwater runoff is not planned.

# FIELD DATA COLLECTION ACTIVITIES AND RESULTS

As a part of the Hydrogeologic Study, on May 13 and 14, 2021, GeoInsight oversaw the drilling of six soil borings completed as groundwater monitoring wells at the Property (GEO-1 through GEO-6). Borings/wells GEO-2, GEO-3, GEO-4, were advanced on the Tuck condo development portion of the Property. Boring/well GEO-5 was located near the proposed future lot line separating the Tuck and Benchmark developments, and GEO-1 and GEO-6 are located on the proposed Benchmark (northern) part of the Property. These six borings/wells, along with pre-existing wells MW-3 and MW-6 associated with the Evolve facility to the north, were used in this Hydrogeologic Study. Boring/well completion logs for GEO-1 through GEO-6 are presented in Attachment B and the locations are illustrated on Figures 1 through 3.

On May 23 and 28, 2021, GeoInsight collected depth to groundwater measurements and water quality indicator parameter readings (pH, temperature, dissolved oxygen, specific conductance, and oxidation-reduction potential) in the eight wells (Tables 1 and 2, respectively). On May 28, 2021, wells GEO-1 through GEO-6 and MW-3 and MW-6 were surveyed relative to a local benchmark (see Figure 2) to establish wellhead elevations for use in determining groundwater flow calculations (Table 1).

Wells GEO-1 through GEO-6, and MW-3 and MW-6 were sampled on May 23, 2021, and samples were analyzed by a laboratory for ammonia-nitrogen, nitrate-nitrogen, and chloride. A copy of the laboratory analytical report is presented in Attachment C and the nitrogen and chloride data are presented in Table 2.

Nitrate and chloride concentrations reported in groundwater samples collected from wells GEO-1 through GEO-6 ranged from not detected above the laboratory reporting limit of 0.1 milligrams per liter (mg/L) to 2.9 mg/L (nitrate) and 3.9 mg/L to 240 mg/L (chloride). In wells MW-3 and MW-6 located at the Evolve facility and upgradient of the Property, reported nitrate and chloride concentrations were 0.9 mg/L and 1.3 mg/L (nitrate) and 420 mg/L and 430 mg/L (chloride).

On May 28, 2021, *in-situ* monitoring well/aquifer hydraulic conductivity testing ("slug tests") were performed at wells GEO-1 through GEO-6. Because the monitoring wells had screens intersecting the water table (not fully submerged), slug-out (falling head) tests were conducted. Hydraulic conductivity values from the slug tests ranged from 23 to 27 feet per day (ft/day). Note, that the aquifer responses recorded in wells GEO-3, GEO-4, and GEO-5 (and for the second test at GEO-2) were too rapid to provide useful data for calculating hydraulic conductivities. Slug test data and charts for wells GEO-1, GEO-2, and GEO-6 are presented in Attachment D.

Previous hydraulic conductivity testing by others in a February 2010 hydrogeologic study report for the Evolve facility to the north reported hydraulic conductivity values from 22 to 250 feet per day. The higher end range in values in that report appear to have been calculated using rapid slug test response data, which tends to yield higher and unrepresentative calculated hydraulic conductivity values. The 22 ft/day value from the Evolve project correlates with the range of results from the GEO-1, GEO-2, and GEO-5 tests.

# HYDROGEOLOGIC SETTING

The topography of the Property is approximately 110 feet to 116 feet above mean sea level (MSL). The Property is generally level with Lafayette Road. The area surrounding the Property is mixed residential and commercial and the Coakley Landfill, which is closed landfill and a USEPA Superfund Site, borders the Property to the west/southwest (see Assessors Map in Attachment A).

Based upon information obtained during the completion of the soil borings at the Property, native soil is primarily a glacial outwash deposit. The site stratigraphy was generally observed to consist of an upper coarse-grained layer (light brown to brown, fine to coarse sand, with some to trace amounts of gravel, and some to trace amounts of silt) and a lower fine-grained layer (fine sand and silt, with little to trace amounts of clay).

Based upon a review of the Bedrock Geologic Map of New Hampshire, bedrock underlying the Property consists of quartz-feldspar granitic gneiss and pegmatite intruded into the Rye formation and forming a migmatite. Outcrops were not observed on the Property and the borings completed did not encounter refusal to explorations depths up to 33 feet below ground surface (bgs; well GEO-6). Refusal on presumed bedrock (subsequently cored for confirmation) at the Evolve facility in borings completed for the 2010 hydrogeologic study for that project, was encountered at depths of 11 feet bgs (northeast part of the Evolve property) and 35 feet bgs (southwest part of Evolve property).

Depth to groundwater in the eight wells gauged on May 23 and 28, 2021 ranged from approximately 13.5 feet bgs (well GEO-2) to 24.5 feet bgs (well GEO-5), which equates to relative elevations of 96.5 feet MSL (well GEO-2) and 93.5 feet MSL (well GEO-5). Groundwater elevation contours were mapped on the development site plan for the Property (Figures 2 and 3). Groundwater was at an elevation of approximately 104 feet at the northeast part of the Property and slopes to an elevation of 93.5 feet at the southwest part of the Property. With respect to the proposed condo development on the southern portion of the Property, groundwater flow is generally directed westerly with a high groundwater elevation of 98 feet at the eastern Property line to 93.5 feet at the western property boundary.

# COAKLEY LANDFILL SUMMARY

As previously mentioned, the Property (Map 10, Lot 1) abuts the Coakley Landfill Superfund site. While groundwater quality beneath the Property does not appear to be affected by conditions at the landfill, the Property is currently recorded in the Groundwater Management Zone (GMZ) for the Coakley site. A copy of the New Hampshire Department of Environmental Services (NHDES)-issued GMP and Notice of GMP recorded at the registry of deeds for the Coakley Landfill are presented in Attachment E. Given the nature of the groundwater conditions at the Superfund site and its proximity to the Property, GeoInsight reviewed available investigation and groundwater monitoring reports for the landfill as a part of this Hydrogeologic Study. The

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following information was obtained from the Draft 2019 Annual Report (dated July 31, 2020) for the Coakley Landfill on file with the NHDES:

"Overburden groundwater flowing westward from the landfill discharges into a large wetland complex that serves as a hydraulic boundary for groundwater and the headwaters for Berrys Brook, which then flows in a northerly direction, and Little River, which flows to the south.

Groundwater flow in bedrock is also interpreted to move in a westerly direction from the landfill toward a bedrock trough located beneath the wetland complex. This bedrock trough is oriented north/northeast to south/southwest parallel to regional geologic structure. As groundwater encounters this bedrock trough, it is likely that groundwater in bedrock is migrating in the direction (trend) of regional geologic structure, which is coincident with the Berrys Brook valley to the north and the Little River valley to the south and ultimately discharging to Little River and Berrys Brook.

Consistent with historical results, CL [USEPA Cleanup Level] and/or AGQS [Ambient Groundwater Quality Standard] exceedances were identified for 1,4-dioxane, TBA [tertiary butyl alcohol], arsenic, and manganese in one or more wells [at and near the landfill]. In general, the parameters and locations that exceeded the regulatory thresholds are similar to historical monitoring events. Tert-butyl alcohol exceedances were limited to two wells in 2019, consistent with historical data."

Groundwater monitoring at the landfill also includes sampling of per- and poly-fluorinated alkyl substances (PFAS) in overburden and bedrock groundwater as PFAS are a constituent of concern at the landfill site. Groundwater elevation contour plans and constituent distribution maps from the aforementioned 2019 Annual Report are presented in Attachment E and the location of the Property is identified on these plans.

The groundwater contour plans for the overburden and bedrock aquifer for the landfill generally depict a western component to groundwater flow. This finding would generally position the Property hydraulically upgradient from the landfill, which is consistent with a mapped westerly groundwater flow direction for the Property based upon wells installed for this Hydrogeologic Study.

Based upon the mapped extent of constituent/plume iso-contours in groundwater for the landfill (Attachment E), arsenic, manganese, and 1,4-dioxane plumes were <u>inferred</u> to be present in overburden groundwater at the Property, and 1,4-dioxane and PFAS were <u>inferred</u> to be present in bedrock groundwater beneath the Property. It should be noted; however, that the iso-contours were inferred by others in the vicinity of the Property based upon data from distant monitoring wells (see well locations on CES Inc.'s Figure 3 and 4 in Attachment E) and are not based on groundwater testing data obtained from the Property (also, Property-specific overburden groundwater flow direction is westerly). Groundwater sampling data from a pre-existing overburden monitoring well on the Property ("unnamed monitoring well" on Figures 2 and 3; currently dry, and unavailable for this study) collected in January 2020 by others had detected concentration of arsenic, manganese, and PFAS, which were below applicable AGQSs (1,4-dioxane was not tested in the January 2020 sampling event).

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Arsenic and manganese are commonly present in groundwater as geologic background consistent with the January 2020 concentrations reported for the unnamed well (9.4 mg/L for arsenic and 260 mg/L for manganese). The detected concentrations of two PFAS', perfluorooctanoic acid (PFOA) of 3.5 parts per trillion or ppt, and perfluorooctane sulfonic acid (PFOS) of 3.94 ppt in the unnamed monitoring well at the Property may possibly be false positives or anthropogenic background, and unrelated to the landfill, but are less than the current AGQSs of 12 ppt for PFOA and 15 ppt for PFOS. This 2020 groundwater testing data furthers the conclusion that the landfill is not adversely affecting overburden groundwater below the Property.

# **GROUNDWATER MOUNDING ANALYSIS**

Depth to groundwater below the Property ranges from 13.5 to 24.5 feet bgs, so mounding of groundwater beneath proposed wastewater leach fields is not anticipated to reduce the unsaturated soil profile such that percolation of groundwater will be hindered. Also, with the proposed porous pavement to manage and reinfiltrate stormwater and with no localized recharge basin planned, mounding due to storm water re-infiltration is not anticipated to be significant. However, following standard practice and to verify that there will be no significant mounding beneath the leach fields, GeoInsight calculated estimated/predicted groundwater mound heights using the proposed design flows and hydraulic conductivity data obtained in conjunction with this study.

The maximum groundwater mound height beneath the wastewater disposal fields was calculated using the method described by Hantush (1967)<sup>1</sup>. A calculation for a single field was conducted to represent each of the ten fields as they all have the same design flows and will be located in similar soil types. Variables in the mounding calculation included:

- Initial saturated thickness: 10 feet. This was based upon soil boring with total depths of approximately 30 feet and a depth to water of approximately 20 feet. Since the borings did not reach refusal on bedrock, the actual saturated thickness is greater than 10 feet, but lower saturated thicknesses result in higher predicted mounds, so this is a conservative assumption.
- Hydraulic conductivity: 23 feet/day. This is the lowest value calculated from the slug tests performed as part of this study. Use of the lower hydraulic conductivity value results in a conservative condition (it will predict higher mound heights).
- Porosity: 0.2 (dimensionless). This is an assumption based upon literature values for the sandy materials described in the boring logs.
- Disposal field dimensions: 42 feet by 16.5 feet. This is the design size of 9 of the 10 fields. The tenth field is designed at 32 feet by 22.5 feet which results in a smaller mound.
- Discharge volume: 960 gallons per day. This is the design volume for each disposal field. The design volume is conservative and typical flows will be lower.

<sup>&</sup>lt;sup>1</sup> Hantush, M.S. 1967, *Growth and decay of groundwater mounds in response to uniform percolation*: Water Resources Research, v.3, P. 227-234.

• Time of loading: 90, 180 and 365 days. These are all extremely conservative conditions. Typically, 30 days is considered the duration required to reach steady-state conditions even at maximum loading.

Results of the mounding calculations gives predicted mound heights of 0.3 feet, 0.7 feet and 1.3 feet for loading durations of 90 days, 180 days and 365 days, respectively, beneath the leach fields (Attachment F). With depths to water on site of 13 to 24 feet or greater, these mound heights are not significant.

# NITRATE LOADING

Leach fields, particularly those that aggregate wastewater flows from multiple dwelling units into shared subsurface disposal systems, can result in a contribution of nitrate into the aquifer that, depending on site hydrogeology, can result in nitrate levels that exceed the New Hampshire AGQS of 10 mg/L. It is important to evaluate the nitrate loading and how that affects groundwater quality, with particular concern to meeting the AGQS of 10 mg/L at the downgradient Property boundary.

The nitrogen/nitrate concentration at the downgradient Property boundary was simulated using a commonly accepted mass-balance approach. In this method, the nitrate concentration is calculated by the total nitrate mass entering the groundwater on the property, divided by the water recharging the area of the wastewater disposal fields that flows to the downgradient boundary plus any known background concentration of nitrate. The total nitrogen/nitrate concentration is given by the volume and concentration of wastewater flows and inputs from loss from fertilized lawn area. There are 10 wastewater disposal fields with a design flow of 960 gallons per day each. A conservative nitrate concentration assumption for residential wastewater is 40 mg/L (Massachusetts DEP *Guidelines for Title 5 Aggregation of flows and Nitrogen Loading* 310 CMR 15.216 cites 35 mg/L). Assuming a post development-maintained lawn area of 1 acre in the wastewater field recharge area (Figure 3), a fertilizer application of 3 pounds per 1,000 square feet per year of which 25% is not consumed and is leached to the groundwater (MADEP *Guidelines*), the total nitrate load to the Property is approximately 545 million milligrams per year.

The area in which groundwater flows to the disposal fields from the upgradient to the downgradient boundary was delineated by interpretation of the May 28, 2021 groundwater contour map (Figure 3). This area was measured at 3.53 acres. As conservative assumption, the pavement, which is proposed to be porous, was assumed for the mass balance calculation to be impermeable. The pavement and building areas totaling 1.72 acres was deducted from the recharge area. This is conservative as permeable/porous pavement and roof run-off recharge via drip edges are planned for the development, so actual recharge to the disposal field recharge area will be higher than simulated. Annual average precipitation for Rye is 50 inches of which it is assumed 50 percent infiltrates to recharge groundwater. Since the water supply is municipal and coming from an off-site source rather than an on-site well, the wastewater fields yield a total net recharge of 17 million liters per year. This results in a calculated concentration of nitrate of 30.4 mg/L plus a known background concentration of an average 1.3 mg/L, which results in 31.7 mg/L of nitrate in groundwater at the downgradient Property boundary. Nitrate loading calculation spreadsheets are presented in Attachment F. The predicted concentration of

31.7 mg/L of nitrate exceeds the NH Ambient Groundwater Quality Standard (NH AGQS) of 10 mg/L and, therefore, denitrification via pretreatment will be necessary.

SeptiTech nitrate pretreatment systems are planned for each disposal field. According to SeptiTech / Bio-Microbics of Maine Inc., their systems will result in 85 to 90 percent reduction in nitrogen/nitrate. Assuming the low-end estimate of 85 percent reduction of nitrogen in effluent from the treatment systems, the nitrogen input to the mass balance calculation was updated substituting 6 mg/L nitrogen in place of the 40 mg/L assumption for untreated residential wastewater effluent. The resulting mass balance calculation (with other inputs remaining the same), yields a concentration of 5.3 mg/L nitrate from the pre-treated wastewater effluent from the SeptiTech systems, plus a known background concentration of an average 1.3 mg/L, for a total predicted nitrate level 6.6 mg/L at the downgradient Property boundary, which is below the NH AGQS of 10 mg/L.

### CONCLUSIONS

Based upon the Hydrogeologic Study completed for the Property, recharge of residential septic wastewater into 10 leach fields in the proposed Tuck condo development, assuming pretreatment with SeptiTech denitrification units, will result in nitrate concentrations that are below the NH AGQS of 10 mg/L at the downgradient (western) Property boundary. This conclusion indicates that the wastewater systems will not cause degradation of the water quality in the Aquifer Protection District or in groundwater migrating off-site.

It should be further noted, notwithstanding, the preceding conclusion, that the Property is located in the GMZ for the Coakley Landfill, which currently restricts use of groundwater on-site, and groundwater from the Property flows towards and onto the Coakley Landfill property, which is also a part of the landfill's GMZ where groundwater use is restricted. Therefore, use of the overburden or bedrock aquifers in the Aquifer Protection District on and in the area of the Property and landfill for a future municipal well location appears unlikely. Nonetheless, the proposed nitrate pretreatment systems for the condo development leach fields are protective of groundwater quality in the Aquifer Protection District.

Please contact us at (603) 314-0820 if you have questions regarding this Hydrogeologic Study.

Sincerely, GEOINSIGHT, INC.

Darrin L. Santos, P.G. Associate/Senior Geologist

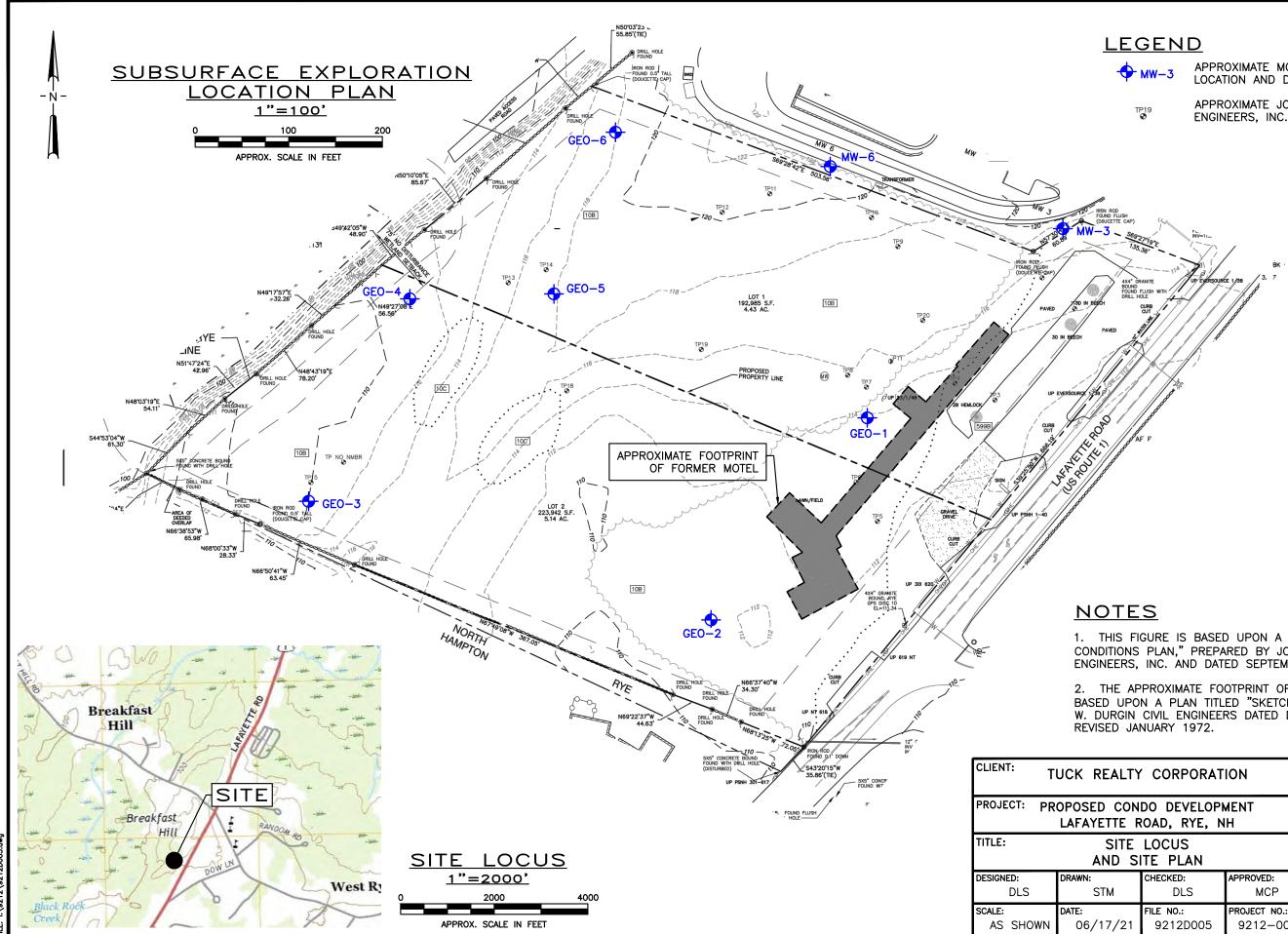
Attachments

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Andrea W. Kenter, P.G. Senior Associate/Senior Hydrogeologist

cc: Tuck Realty Corporation P:\9212-007 Tuck Realty Rye NH Hydro Study\Rye Tuck Realty Hydro study.doc FIGURES

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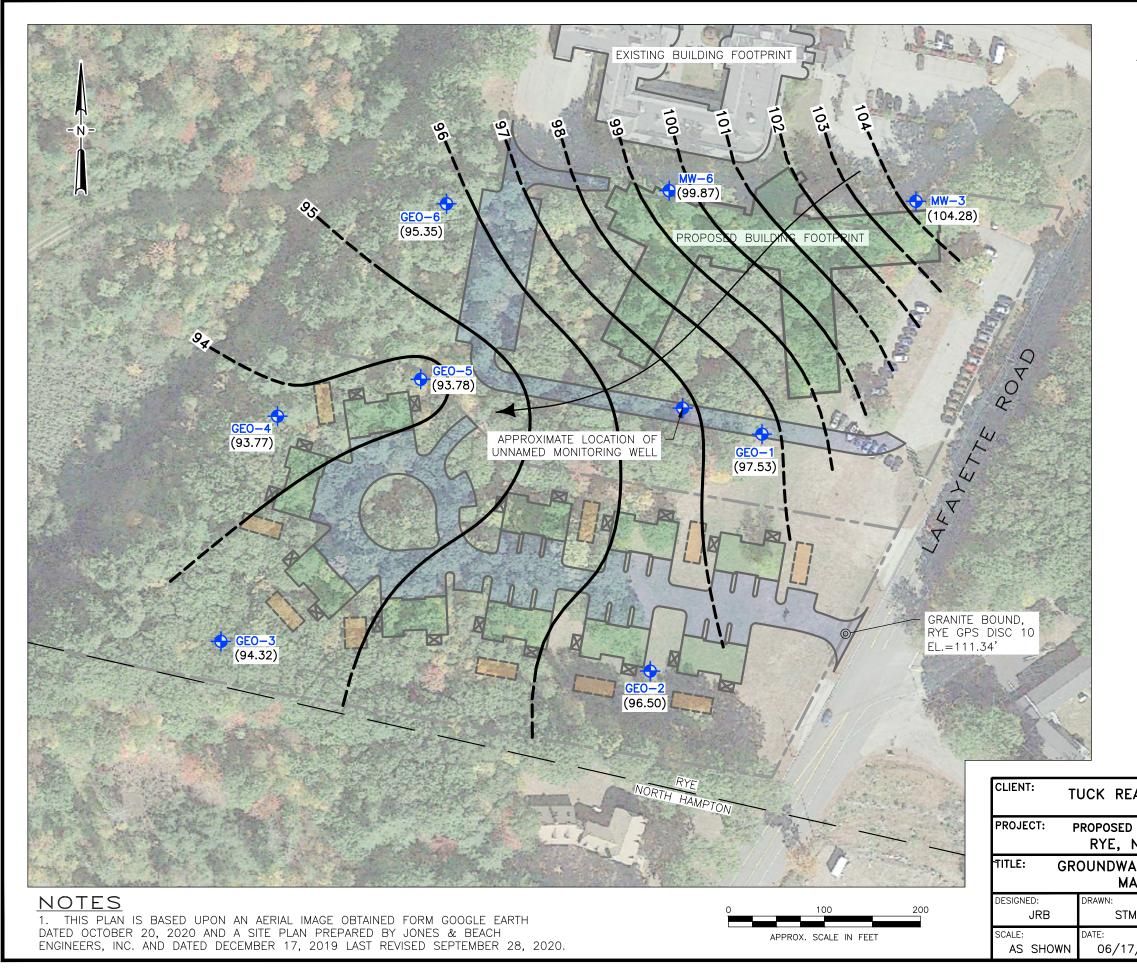
APPROXIMATE MONITORING WELL LOCATION AND DESIGNATION

APPROXIMATE JONES & BEACH ENGINEERS, INC. TEST PIT LOCATION

1. THIS FIGURE IS BASED UPON A PLAN TITLED "EXISTING CONDITIONS PLAN," PREPARED BY JONES & BEACH ENGINEERS, INC. AND DATED SEPTEMBER 28, 2020.

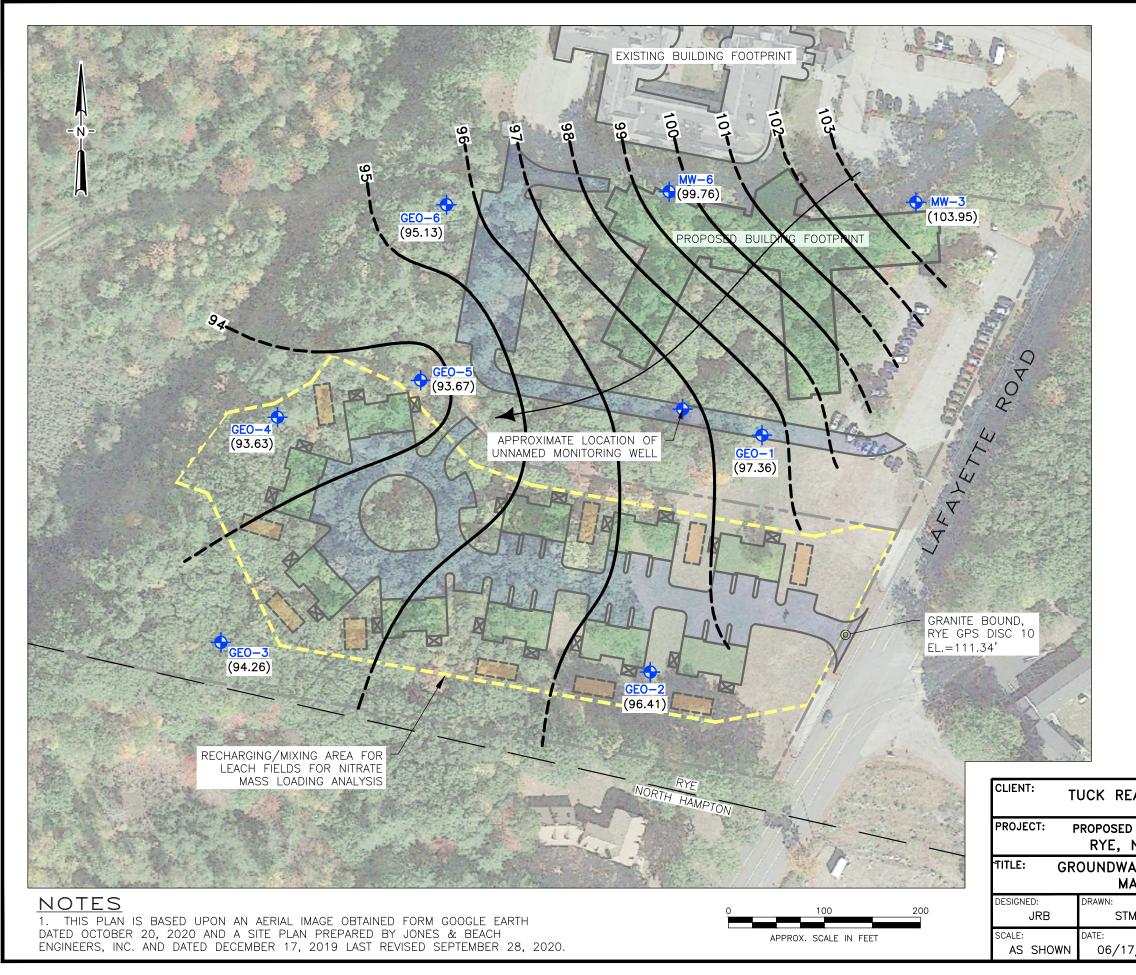
2. THE APPROXIMATE FOOTPRINT OF THE FORMER MOTEL IS BASED UPON A PLAN TITLED "SKETCH OF LAND," BY JOHN W. DURGIN CIVIL ENGINEERS DATED DECEMBER 1971 AND

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LEGEND	-
	APPROXIMATE PROPERTY BOUNDARY
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LEGEND	-
	APPROXIMATE PROPERTY BOUNDARY
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TABLES

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# TABLE 1 GROUNDWATER ELEVATION DATA MAP 10, LOT 1 LAFAYETTE ROAD RYE, NEW HAMPSHIRE

Well ID	Date	TOC Elevation (feet)	Depth To Water (feet)	Groundwater Elevation (feet)
	5/23/2021		19.05	97.53
GEO-1	5/28/2021	116.58	19.22	97.36
	5/23/2021		16.47	96.50
GEO-2	5/28/2021	112.97	16.56	96.41
	5/23/2021		17.05	94.32
GEO-3	5/28/2021	111.37	17.11	94.26
	5/23/2021		20.14	93.77
GEO-4	5/28/2021	113.91	20.28	93.63
	5/23/2021		27.25	93.78
GEO-5	5/28/2021	121.03	27.36	93.67
	5/23/2021		24.91	95.35
GEO-6	5/28/2021	120.26	25.13	95.13
	5/23/2021		16.98	104.28
MW-3	5/28/2021	121.26	17.31	103.95
	5/23/2021		23.59	99.87
MW-6	5/28/2021	123.46	23.70	99.76

# NOTES:

1. TOC = top of casing.

2. TOC elevations were surveyed by GeoInsight, Inc. on May 28, 2021 to an benchmark with an established elevation of 111.34 feet (granite bound with a "Rye GPS" disc note on it) for the survey datum/control.

### TABLE 2 GROUNDWATER FIELD AND LABORATORY TESTING DATA MAP 10, LOT 1 LAFAYETTE ROAD RYE, NEW HAMPSHIRE

			FI	ELD TEST PARAM	ETERS		LABO	RATORY AN	ALYSES
Well ID	Date	Temp	рН	Specific Conductivity	Dissolved Oxygen	Oxidation-Reduction Potential	Ammonia- Nitrogen	Nitrate- Nitrogen	Chloride
		(celcius)	(standard units)	(milli-Siemens per centimeter)	(mg/L)	(milli-Volts)	(mg/L)	(mg/L)	(mg/L)
				NH Ambient	Groundwater (	Quality Standard (AQGS)	No Standard	10 mg/L	No Standard
GEO-1	5/23/2021	13.8	7.8	928	2.2	72	ND(0.5)	ND(0.1)	220.0
GEO-I	5/28/2021	10.4	6.8	1,166	12.6	227			
CEO A	5/23/2021	10.4	6.6	191	8.3	22	ND(0.5)	2.2	3.9
GEO-2	5/28/2021	8.5	6.6	255	7.6	206			
CEO A	5/23/2021	10.9	6.8	780	8.5	29	ND(0.5)	1.1	200
GEO-3	5/28/2021	8.8	6.6	935	7.4	207			
	5/23/2021	10.5	6.7	382	8.8	30	ND(0.5)	1.4	76
GEO-4	5/28/2021	8.5	6.6	384	8.3	197			
CEO -	5/23/2021	10.7	6.6	111	8.5	-1	0.9	ND(0.1)	12
GEO-5	5/28/2021	8.6	6.8	117	7.8	192			
CEO (	5/23/2021	12.1	6.3	890	8.4	-7	ND(0.5)	2.9	240
GEO-6	5/28/2021	10.4	6.2	1,132	7.6	200			
	5/23/2021	11.5	5.6	1,378	9.4	67	ND(0.5)	1.3	420
MW-3	5/28/2021	9.4	5.7	2,008	8.7	200			
	5/23/2021	12.4	6.4	1,437	9.6	73	ND(0.5)	0.9	430
MW-6	5/28/2021	10.3	6.4	1,714	8.2	196			

Notes:

1. ND(x) denotes analyte not detected above laboratory practical quantitation limit noted in parentheses.

2. mg/L = milligrams per liter.

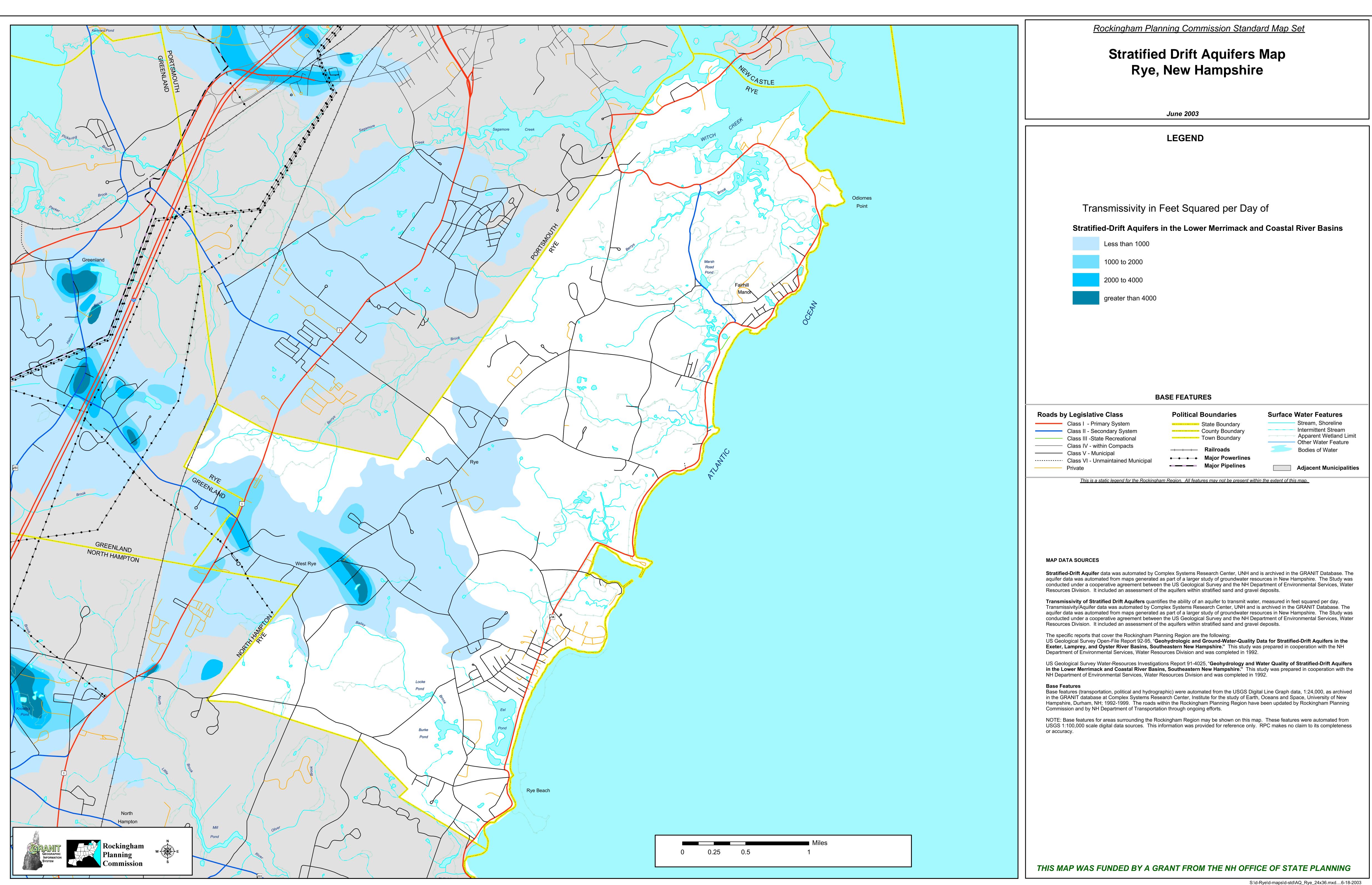
# ATTACHMENT A

# ASSESSOR MAP AND AQUIFER PROTECTION DISTRICT MAP

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Data shown on this map is provided for planning and informational purposes only. The municipality and CAI Technologies are not responsible for any use for other purposes or misuse or misrepresentation of this map.



# ATTACHMENT B

# SOIL BORING / WELL COMPLETION LOGS

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PTH		SAMPLE				<u> </u>	ELL	00,20,2021		FIELD	.90	
(ft)		Pen/Rec					LETION		IPLE	STRATUM	SCREENING	NOT
10)	#	(in)	(ft)	Blov	vs/6''		TAIL	DESCR	IPTION	DESCRIPTION	(ppm)	
0 -		(111)	(11)		-			0-2" Organic topsoil			(ppm)	
					-			5 2 Organic topson				
1 -		L			-							
					-							
2 -												
					-							
3 -					-	100000000000000000000000000000000000000		Crinding -+ 2!				
								Grinding at 3'				
4 -												
					-							
5 -	G	04/12				100000000000000000000000000000000000000					<u> </u>	
	S-1	24/12	5-7		7			S-1: Dense, Brown, fine to			<1	1
6 -					7			Gravel, trace organics, dar	np			
					9							
7 -					6							
					-			Cuttings: Gravelly from 6-	7'	SAND		
8 -												
				-								
9 -					-	1202020202020202020						
-				-	-							
10 -					-							
	S-2	24/12	10-12		8			S-2: Medium dense, brown	0.1		<1	1
11 -				1		100000000000000000000000000000000000000		SAND, little Silt, trace Gra	wel, damp			
					2							
12 -					3							
					-							
13 -					-							
					-							
4 -					-							
				-	-							
15 -				-	-							
	S-3	24/18	15-17		)			S-3: Dense, brown, fine to	coarse SAND, some Silt,		<1	1
6 -					7			trace Gravel, moist				
					7							
17 -					1						├	
										SAND & SILT	└─────┨	
18 -					-				10.10		└─────┨	
					-			Cuttings: Gravelly between	1 18-19'		└─────┨	
9 -					-							
					-							
20 -		CRAT			-		N/F					
GRANULAR SOILS						COHES		WELL	WELL	INTERVAL		NID
	D				Dla	SOIL		CONSTRUCTION	MATERIALS	(feet bgs)	LEGE	ND
	Blows/ft.Density0-4V. LOOSE				Blows		soft	NOTES	C	0.05		
		0-4			<2		. SOFT		Concrete	0-0.5		
		5-10	LOO M DE		2-4		SOFT		Backfill	0.5-12		
		11-30	M. DE		5-8		. STIFF	32' well constructed with	Grout	NA 12.12		
		31-50	DEN		9-15		STIFF	3' standpipe and 29' bgs.	Bentonite: Chips	12-13		
		>50	V. DE	INSE	16-3		. STIFF		Sandpack: # 2 Sand	13-29		
					>30	I	IARD		Riser	17		
	1		1			1			Screen	15		

		0	Client	Bench	mark S	enior	iving / T	uck Res	alty Corp.	Boring Identification: B-	9 W	ell ID: GEO-1	
Geo	oIns	ight	Project:							boring fuentification. D-			2
vironmenta	l Strategy	& Engineering							-)	Chkd. By: DLS		oject Number: 9	
		any: GeoS							ing Location: 43.002	43721 N 70.81120395 W			
oreman								Тор	of PVC Riser Elevat	ion: 116.58'	Da	tum: 111.34'	
eoInsig	ht Eng	gineer/Geo	ologist: Jo	oshua B	rown			Тор	of Protector Elevation	on: NS	Gi	round Elevation:	NA
								Dat	e Started: 5/13/2021			te Completed: 5	/13/2021
		LING ME	THOD				PLER			GROUNDWATER M			
ehicle: A							/ Auto		Date	Depth (ft)	Reference	Stabiliz	
lodel: C					Hamn Fall (i		): 140	_	05/13/2021	19.03	Top of Riser	1 ho	
		w stem aug				<i></i>			05/23/2021	19.05	-	10 da	lys
EPTH (ft)	#	Pen/Rec	Depth	Blow		COM	WELL IPLETIC ETAIL	ON		IPLE IPTION	STRATUM DESCRIPTION	FIELD SCREENING	NOTE
20 -	64	(in)	(ft)	4		D	EIAIL	S 4	Madium danca anar	fine SAND and SILT trace		( <b>ppm</b> )	1
	S-4	24/24	20-22	5					y, wet	fine SAND and SILT, trace		<1	1
21 -				7				Cia	,				
		1		6									
22 -				-									
22				-	-								
23 -			_	-	-								
24 -				-	-								
- ·				-							SAND & SILT		
25 -	a -	24/24	05.05	-				~ ~		an			-
	S-5	24/24	25-27	2 2						ne SILT, trace fine Sand,		<1	1
26 -				3				trac	e Clay, wet			├	
				9				A110	ered to 29' bgs.				
27 -				-				лив	,erea to 27 0gs.				
20		<u> </u>		-									
28 -				-	-								
20				i	-					ated at 29' bgs.			
29 -									Set monitoring				
30 -													
												├────┨	
31 -													
												├	
32 -													
33 -													
24													
34 -													
35 -													
36 -												<b> </b>	
37 -													
												├	
38 -													
39 -													
40 -													
TU		GRAN			(		SIVE		WELL	WELL	INTERVAL		
		SO				SO			CONSTRUCTION	MATERIALS	(feet bgs)	LEGE	ND
	Bl	ows/ft.	Dens		Blows		onsisten		NOTES		· - ·		
		0-4 5-10	V. LOO LOO		<2 2-4		V. SOFT SOFT			Concrete	0-0.5		
		5-10 11-30	M. DE		2-4 5-8		SOF1 M. STIFF	-		Backfill Grout	0.5-12 NA		
		31-50	DEN		9-15		STIFF	32'	well constructed with	Bentonite: Chips	12-13		
		>50	V. DEN		16-3		V. STIFF	3's	standpipe and 29' bgs.	Sandpack: # 2 Sand	13-29		
					>30		HARD			Riser	13-25		
			1			1				Screen	15		

~ -	-	0	Client:	Bench	mark Se	enior Living / Tuc	k Realty Corp.	Boring Identification: B-	-10 W	ell ID: GEO-2	
Geo	oIns					(former Hector's				neet: 1 of	1
						ad (Rt. 1), Rye, N		Chkd. By: DLS	Pr	oject Number: 9	
		any: GeoS	earch, Inc	×		•	Boring Location: 43.001				
reman							Top of PVC Riser Eleva			atum: 111.34'	
oInsig	ht Eng	gineer/Geo	logist: Jo	oshua B	Brown		Top of Protector Elevati	on: NS		round Elevation	
							Date Started: 5/13/2021			ate Completed: 5	5/13/2021
		LING ME	THOD			SAMPLER		GROUNDWATER M	r		
nicle:						2" SS / Auto	Date	Depth (ft) 16.32	Reference	Stabiliz	
	CME-8					ner (lb): 140	05/13/2021 05/23/2021	Top of Riser	1 ho		
PTH		w stem aug		IATIO	Fall (in	WELL	03/23/2021	16.47		10 da FIELD	ays
ft)		Pen/Rec				COMPLETION	SAN	IPLE	STRATUM	SCREENING	NOT
	#	(in)	Depth (ft)	Blov	vs/6''	DETAIL	DESCH	IPTION	DESCRIPTION	(ppm)	nor
0 -		(111)	(11)	-	-		0-2" - Organic topsoil			(PP)	
				-							
1 -				-							
2 -				-							
2 -				-							
3 -				-							
1 -											
5 -	G 1	04/10	57				G1 D	c			
	S-1	24/12	5-7		9		S-1: Dense, grayish brown some Gravel, trace Silt, da			<1	1
6 -					.2		some Gravel, trace Silt, da	шћ			
					.9		Cuttings: Gravelly from	~5-6' and grinding at ~8'			
7 -							Cuttings. Graveny Hom	5.6 and grinning at ~6	SAND &		
0									GRAVEL		
8 -				-							
9 -				-							
1				-							
10 -											
	S-2	24/12	10-12		.3		S-2: Dense, grayish brown			<1	1
11 -					4		soime Gravel, trace Silt, d	ump			
					.8						
12 -					.3						
13 -					-						
					-						
14 -	İ	1	1								
15 -									L		
	S-3	24/18	15-17		2			n, fine to coarse SAND and	<b></b> _	<1	1
6 -					.3		GRAVEL, some Silt, wet				
-					.5						
17 -					9						
8 -					-						
					-				SAND & SILT		
- 19	1										
				-			S-4A: Medium dense, bro	wn, fine to coarse SAND,			
20 -	S-4A	12/12	20-21		5		trace Silt, wet	,		<1	1
21 -					6			ish brown, fine SAND and			
	S-4B	12/12	21-22		.0		SILT, wet			<1	1
22 -	ļ			1	0			ated at 22' bgs.			
							Set monitoring	well at 22' bgs.			
3 -											
24 -											
25 -		GRAN	ULAR		(	COHESIVE	WELL				
		SO				SOILS	CONSTRUCTION	WELL MATERIALS	INTERVAL (foot hog)	LEGH	END
	B	lows/ft.	Dens	sity	Blows			MATERIALS	(feet bgs)		
		0-4	V. LO		<2	V. SOFT		Concrete	0-0.5		
		5-10	LOO		2-4			Backfill	0.5-5		
		11-30	M. DE		5-8		25' well constructed with	Grout	NA		
		31-50	DEN		9-15		3' standpipe and 22' bgs.	Bentonite: Chips	5-6		
		>50	V. DE	NSE	16-30		11	Sandpack: # 2 Sand	6-22		
					>30	HARD		Riser	10		
	1		1		1	1		Screen	1.3		

2. bgs = below ground surface.

	Jne	ighť						k Realty Corp.	Boring Identification: B-		ell ID: GEO-3	
reo	01115	& Engineering					er Hector's	,	Chi-J D., DI C		neet: 1 of	1
		any: GeoS			ette Ko	ad (Rt.	1), Rye, N	Boring Location: 43.001	Chkd. By: DLS	ri	oject Number: 9	9212
	: Mik	•	caren, me	·•				Top of PVC Riser Elevat		De	atum: 111.34'	
		gineer/Geo	logist: Jo	oshua B	rown			Top of Protector Elevatio			round Elevation	: NA
8		,						Date Started: 5/13/2021			ate Completed: 5	
Γ	ORIL	LING ME'	ГНОД		5	SAMP	LER		GROUNDWATER M			
le: A	ΑTV				Type:	2" SS /	Auto	Date	Depth (ft)	Reference	Stabiliz	zation
el: Cl	ME-8	50			Hamm			05/13/2021	16.96	Top of Riser	1 ho	our
od: I		w stem aug			Fall (iı	<b>n):</b> 30		05/23/2021	17.05	Top of Kisei	10 da	ays
ГН	5	SAMPLE 1	INFORM	IATIO			ELL	SAM	PLE	STRATUM	FIELD	
)	#	Pen/Rec	-	Blow	vs/6''		PLETION	DESCR		DESCRIPTION	SCREENING	NO
-		(in)	(ft)				TAIL				(ppm)	
-					-		1010101010101010101	0-3" - Organic topsoil				
+					_							
-					-							
+					-							
ŀ				-	-							
1					-							
Ī				-	-							
Ť				-	-							
1					-							
Ţ	S-1	24/12	5-7		2			S-1: Medium dense, brown	, , ,		<1	1
ļ					7			some Gravel, trace Silt, dar	np			
╞				1	1				1			
ł					) -			Cuttings: Gravelly and grin	ding at ~5'		├────┤	
ŀ					-							
t		1			-							
ŀ				-	-							
†				-	-			1				
ſ				-	-							
T	S-2	24/11	10-12		5			S-2: Medium dense, brown			<1	1
ļ					2			some Gravel, trace Silt, dar	np	SAND &		
ŀ				1				1		GRAVEL		
ł					1			Cuttinger Consults from 10	15		├────┤	
ŀ					-			Cuttings: Gravelly from 10	-13.			
t					-							
ľ				-	-							
Ţ				-	-							
Ţ					-							
ļ	S-3	24/8	15-17		5			S-3: Medium dense, brown	, fine to coarse SAND and		<1	1
+					2			GRAVEL, trace Silt, wet				
ŀ					0 7						├────┤	
ł					-							
ŀ					-							
t					-							
t				-	-							
t				-	-							
Ţ					-							
	S-4	24/18	20-22		6			S-4: Dense, brown, fine to	coarse SAND, some		<1	1
ļ					0			Gravel, some Silt, wet				
ŀ					6 6			Domin - tom	ited at 22' has			
ł				1	v I			Boring termine Set monitoring			├────┤	
ŀ								Set monitoring				
t												
Ī												
Ť												
ļ												
		GRAN			C	OHES		WELL	WELL	INTERVAL		
SOILS Blows/ft. Density				ity	Blows/	SOII	.S nsistency	CONSTRUCTION NOTES	MATERIALS	(feet bgs)	LEGE	LIND
Blows/ft.Density0-4V. LOOSE				<2 store sto		/. SOFT	10110	Concrete	0-0.5			
0-4 V. LOOSE 5-10 LOOSE		2-4		SOFT		Backfill	0.5-5					
	11-30 M. DENSE 5-8 M. STIF				0.51 11	Grout	NA					
				STIFF	25' well constructed with	Bentonite: Chips	5-6					
		31-50         DENSE         9-15         STIFF           >50         V. DENSE         16-30         V. STIFF				3' standpipe and 22' bgs.	Sandpack: # 2 Sand	6-22				
					>30		HARD		Riser	10		
									Screen	15		
ES												

_		•	Client:	Benchr	nark Se	enior Living / Tuc	k Realty Corp.	Boring Identification: B	-12 W	ell ID: GEO-4	
Geo	oIns					(former Hector's		0		eet: 1 of	2
ironmenta	al Strategy	& Engineering				ad (Rt. 1), Rye, N		Chkd. By: DLS	Pr	oject Number: 9	212
		any: GeoS					Boring Location: 43.002			3	
<u> </u>	: Mik						Top of PVC Riser Elevat		Da	tum: 111.34'	
		gineer/Geo	alogist. Id	oshua B	rown		Top of Protector Elevation			ound Elevation:	NA
B				, shuu D	10.011		Date Started: 5/14/2021			te Completed: 5	
1	UBII I	LING ME	THOD	I		SAMPLER	Date Started: 5/14/2021	GROUNDWATER M		-	14/2021
hicle: 4			THOD	-		2" SS / Auto	Date		Reference	Stabiliz	ation
	CME-8	50				er (lb): 140	05/14/2021	Depth (ft)	Kelerence	1 hou	
					Fall (in		05/23/2021	20.05	Top of Riser		
		w stem aug				/	05/25/2021	20.14	_	9 day	/S
CPTH	2	SAMPLE			N	WELL	SAN	IPLE	STRATUM	FIELD	Nom
(ft)	#	Pen/Rec	-	Blow	s/6''	COMPLETION	DESCR	IPTION	DESCRIPTION	SCREENING	NOTE
0 -		(in)	(ft)			DETAIL				(ppm)	
					-		0-3" - Organic topsoil				
1 -					-						
1					-						
2 -					<u> </u>						
					-						
2					-						
3 -					-		Grinding from ~3-5' - Grav	elly.			
,					-		, , , , , , , , , , , , , , , , , , ,	-			
4 -											
_		1			.						
5 -	S-1	24/13	5-7	7	,		S-1: Medium dense, gravis	h brown fine to coarse		<1	1
	0-1	21/15	57	10			SAND, some Gravel, trace			<u></u>	
6 -				9	-		SAND, some Graver, trace	Sin, damp			
				9							
7 -											
							Cuttings: Gravelly from ~5	)-/			
8 -											
					-						
9 -					-						
-					-						
10 -					-				SAND &		
	S-2	24/16	10-12	9			S-2: Medium Dense, grayi		GRAVEL	<1	1
11 -				8			SAND, trace Silt, trace Gr	avel, damp			
				8							
12 -				8	3						
12 7					-		Cuttings: Gravellyl at ~12'	bgs.			
13 -					-						
. 3 -					-						
					-						
14 -					-						
15 -	S-3	24/2	15-17	8	3		S-3: Medium dense, brow	n fine to coarse SAND		<1	1
	5-5	21/2		9			trace Silt, damp	,		~~	
6 -				7							
				1						├	
17 -			+							╞────╂	
										├	
8 -											
19 -										├────┨	
										⊦ I	
20 -											
1	GRANULAR					COHESIVE	WELL	WELL	INTERVAL		
		SO				SOILS	CONSTRUCTION	MATERIALS	(feet bgs)	LEGE	ND
				Blows/		NOTES					
		0-4	V. LO		<2	V. SOFT		Concrete	0-0.5		
		5-10	LOO	SE	2-4	SOFT		Backfill	0.5-10		
	1	11-30	M. DE	NSE	5-8	M. STIFF	30' well constructed with	Grout	NA		
	3	31-50	DEN	SE	9-15	STIFF		Bentonite: Chips	10-11		
		>50	V. DE	NSE	16-30	V. STIFF	3' standpipe and 27' bgs.	Sandpack: # 2 Sand	11-27		
					>30			Riser	15		
			1			1	1	Screen	15		

	C	)				SC	DIL I	BOR	RING / WELL CO	<b>MI</b>	PLETION LOG			
_	-		Client:	Bench	mark S	enior	Living	/ Tuc	k Realty Corp.	I	Boring Identification: B	-12 W	ell ID: GEO-4	
Geo	oIns	sight	Project:				-						eet: 2 of	2
nvironmental	l Strategy	& Engineering	Location							(	Chkd. By: DLS	Pı	oject Number: 9	
Orilling (	Compa	any: GeoS						<u> </u>	Boring Location: 43.0					
Foreman	: Mik	e D.							Top of PVC Riser Elev	vatio	<b>n:</b> 113.91'	Da	atum: 111.34'	
GeoInsig	ht Eng	gineer/Geo	ologist: Jo	oshua I	Brown				Top of Protector Eleva	ation	: NS	G	round Elevation:	NA
	``					_			Date Started: 5/14/202	21		D;	ate Completed: 5	/14/2021
I	DRIL	LING ME	THOD			SAMI	PLER				GROUNDWATER M	IEASUREMENTS	5	
ehicle: A	ATV				Type:				Date		Depth (ft)	Reference	Stabiliz	ation
Model: C			_		Hamn			)	05/14/2021		20.05	- Top of Riser	1 ho	ur
Aethod:		w stem aug			Fall (i	<b>n):</b> 3(	)		05/23/2021		20.14	T op of Kiser	9 da	ys
DEPTH	<b>.</b>	SAMPLE	INFORM	IATIO	N	,	WELL		c.	AMP	ЭГЕ	STRATUM	FIELD	
(ft)	#	Pen/Rec	Depth	Ploy	ws/6''	COM	IPLET	TION			PTION	DESCRIPTION	SCREENING	NOTE
20	#	(in)	(ft)	DIOV	15/0	D	ETAI	L	DES			DESCRIPTION	(ppm)	
20	S-4	24/15	20-22		5				S-4: Medium dense, gra	ayish	brown, fine to coarse		<1	1
21					7				SAND, some Gravel, tra	ace S	ilt, wet			
~1					1									
22				1	3									
~~ -												SAND &		
23												GRAVEL		
23				-										
24				-										
24 -				-										
25				-										
25	S-5	24/6	25-27	1	0				S-5: Medium dense, gra	ay, SI	LT and fine to coarse	Г	<1	1
26				1	0				SAND, wet			CAND 0 OF		
26				1	0							SAND & SILT		
27				1	1				Boring tern	ninat	ed at 27' bgs.			
27 -				-							vell at 27' bgs			
20				-						-	-			
28				-										
20				-										
29 -														
20														
30 -														
31														
51														
32														
52														
33														
55														
34														
54														
35														
33	S-3	24/	15-17											
36														
50														
37														
57														
38														
20														
39														
					]									
40		CDAN	ULAR			COUL	ESIVE		WELL					
		GRAN SO				SOI			CONSTRUCTION		WELL	INTERVAL	LEGE	ND
ŀ	PI	lows/ft.	Dens	itv	Blows		Consist	enev	NOTES		MATERIALS	(feet bgs)	LEGE	1 (D
		0-4	V. LO		2	C	V. SO		NOTES		Concrete	0-0.5		
		0-4 5-10	LOO		<2 2-4		V. SO SOF			⊢	Concrete			
		5-10 11-30	M. DE		2-4 5-8		M. ST			⊢	Backfill	0.5-10 NA		
									30' well constructed wi	ith	Grout	NA 10.11		
	-	31-50	DEN		9-15		STIF		3' standpipe and 27' bg		Bentonite: Chips	10-11		
		>50	V. DE	NOE	16-3		V. ST			⊢	Sandpack: # 2 Sand	11-27		
					>30		HAR	U		H	Riser Screen	15 15		

_		0	Client	Bench	mark S	enior Living / Tuc	RING / WELL CON	Boring Identification: B-	.13 W	ell ID: GEO-5	
Geo	Ins	- ighť				1 (former Hector's		Doring Identification. D-			2
onmental s	Strategy	& Engineering				oad (Rt. 1), Rye, N		Chkd. By: DLS		oject Number: 9	
		ny: GeoS				Jau (Rt. 1), Ryc, R	Boring Location: 43.002			oject rumber.	212
eman:		•	caren, me	•			Top of PVC Riser Eleva		De	atum: 111.34'	
		gineer/Geo	logist. Id	shua F	Brown		Top of Protector Elevati			round Elevation	• NA
margn	ti Dhe	sincer/oet	nogist. st	J311ua 1	JOWI		Date Started: 5/14/2021	<b>011.</b> 145		ate Completed: 5	
D	RILI	LING ME	THOD			SAMPLER	Dute Started, 5/11/2021	GROUNDWATER M			/11/2021
icle: A						2" SS / Auto	Date	Depth (ft)	Reference	Stabiliz	ation
del: CN		50				ner (lb): 140	05/14/2021	27.11		1 ho	
hod: H	Iollov	v stem aug	er		Fall (i		05/23/2021	27.25	Top of Riser	9 da	ys
РТН		SAMPLE		<b>IATIO</b>		WELL		•		FIELD	
ft)		Pen/Rec	Depth	DI	1611	COMPLETION		APLE	STRATUM	SCREENING	NOT
	#	(in)	(ft)	Blov	vs/6''	DETAIL	DESCI	RIPTION	DESCRIPTION	(ppm)	
)			, í	-	-		0-3" - Organic topsoil				
				-							
t t				-							
				-							
Ť				-							
T							Cuttings: Grinding at ~2	- Gravelly material			
T				-							
Ĺ	S-1	24/12	5-7		9		S-1: Dense, brown, fine to			<1	1
; _					2		· · ·	amount of pulverized rock			
Ľ					20		and roots in sampler.				
, .				1	.3						
Т				-							
T T											
				-							
L				-							
0											
Ĺ	S-2	24/13	10-12		5		S-2: Medium dense, grayi			<1	1
1					9		SAND, trace Silt, trace G	avel, damp			
⊢					7						
2 -					6						
F									SAND		
3 -											
F											
4 -											
⊢											
5 -	63	24/12	15-17		5		S 2. Madium James	ah heaven fina to occorr		<1	1
ŀ	S-3	24/12	13-17		5 9		S-3: Medium dense, grayi SAND, trace Silt, damp	sn brown, nne to coarse		<1	1
5 -					2		SAND, uace Sill, uainp				
ŀ					2						
7 -					-						1
ŀ					-		1				1
8 -					-						1
9 -											
. F											
0 -		GRAN	ULAR		(	COHESIVE	WELL				
		SO				SOILS	CONSTRUCTION	WELL	INTERVAL	LEGH	END
	Bl	ows/ft.	Dens	ity	Blows		NOTES	MATERIALS	(feet bgs)		
F		0-4	V. LO		<2			Concrete	0-0.5		
		5-10	LOO		2-4			Backfill	0.5-15		
		11-30	M. DE		5-8		251 11	Grout	NA		
		31-50	DEN		9-15		35' well constructed with	Bentonite: Chips	15-16		
		>50	V. DE		16-3		3' standpipe and 32' bgs.	Sandpack: # 2 Sand	16-32		
					>30	HARD		Riser	17		
	>50 HARD						•		15		

_		9	Client:	Bench	mark S	enior I	iving /	Tuc	k Realty Corp.		Boring Identification: B	-13 W	ell ID: GEO-5	
Geo	oIns	_ ighť	Project:								Doring ruthinitiation D			2
ironmenta	l Strategy	& Engineering	Location	• Lafa	vette R	ad (P	1) R.	e N	н		Chkd. By: DLS		oject Number: 9	
		ny: GeoS			sene Re		1 <i>)</i> , N	U, 19			60300 N 70.81252969 W		oject i tullioci , y	_1_
	: Mike		caren, me	·•					Top of PVC Riser Ele			De	tum: 111.34'	
		ineer/Geo	Jogist. L	oshua B	Prown				Top of Protector Eleva				round Elevation:	NΛ
JIIISIE	nt Eng	,meen/oeu	nogist. st	Joinua L	nown				Date Started: 5/14/202		<b>u.</b> 145		te Completed: 5	
1		LING ME	TUOD			SAMF	IFD		Date Started. 3/14/202	-1	GROUNDWATER M			14/2021
icle: 4		JING ME	шор		Type:	-			Date	- 1		Reference	Stabiliz	otion
	ME-85	0			Hamn				05/14/2021		Depth (ft)	Kelefence	1 hou	
					Hamn Fall (i				05/23/2021		27.11	Top of Riser	9 dav	
		v stem aug				<i></i>			05/25/2021		27.25			/S
PTH	2	AMPLE		IATIO.	N		VELL		S	AM	PLE	STRATUM	FIELD	NOT
ft)	#	Pen/Rec	-	Blow	vs/6''		PLET		DES	CRI	IPTION	DESCRIPTION	SCREENING	NOT
- 0		(in)	(ft)		-	D	ETAIL	1					(ppm)	
	S-4	24/3	20-22	1						e to o	coarse SAND, trace Silt,		<1	1
1 -				1	-				trace Gravel, moist					
					7									
2 -				2										
, i				-	-									
3 -				-	-									
2				-	-				Cuttings: Grinding at ~	23' t	ogs.			
4 -				-	-									
7]				-	-									
5 -				-	-									
	S-5	24/10	25-27	1	1				S-5: Medium dense, br	own	ish gray, fine to coarse		<1	1
.6 -				ç	)				SAND, some Gravel, tr	ace	Silt, wet	SAND &		
.0 -				1	0							GRAVEL		
.7 -				e	5									
./ -				-	-									
0				-	-									
-8				-	-									
0				-										
- 9				-	-									
				-	-									
- 30	S-6	24/	30-32	1	6				S-6: Medium dense, br	own	ish gray, fine to coarse		<1	1
				1	4				SAND, some Gravel, tr		0.1			
31 -				1	4									
32 -				2	0						ted at 32' bgs.			
,2 -											well at 32' bgs			
33 -														
· · · ·														
4 -														
-+														
_														
5 -														
6 -			1											
_														
7 -														
8 -														
i9 -														
- 0		GRAN	ULAR			COHE	SIVE		WELL	ļ				
		SOI				SOI			CONSTRUCTION		WELL	INTERVAL	LEGE	ND
	Bl	ows/ft.	Dens	sitv	Blows		onsiste	ncv	NOTES		MATERIALS	(feet bgs)	21.01	
		0-4	V. LO		<2	_	V. SOF	v			Concrete	0-0.5		
		5-10	LOO		2-4		SOFT			ŀ	Backfill	0.5-15		
		1-30	M. DE		5-8		M. STI			ŀ	Grout	NA		
		31-50 81-50	DEN		9-15		STIFF		35' well constructed w		Bentonite: Chips	15-16		
		>50	V. DEN		16-3		V. STIF		3' standpipe and 32' bg	gs.		16-32		
		-50	v. DE	TIOL:	>30		V. STIE HARE			ŀ	Sandpack: # 2 Sand	10-32		
					>30		ΠΑΚL	,		ļ	Riser Screen	17		
			1			1								

Soil samples screened in the field with a MiniRae 3000 photoionization detector with a 10.6 eV lamp.
 bgs = Below ground surface; NS = Not surveyed; WOH = Weight of hammer

_		0	Client	Bench	mark S	enior Living / Tuc	k Realty Corp.	Boring Identification: B	-14 <b>w</b>	ell ID: GEO-6	
Geo	Jns	sight				l (former Hector's		2 51 mg Iuchantauon. D			2
ronmenta	l Strategy	& Engineering				ad (Rt. 1), Rye, N		Chkd. By: DLS		oject Number: 9	
		any: GeoS			yelle K	Dau (Kl. 1), Kye, N	Boring Location: 43.003		11	ojett Nulliber. 9	212
			earcn, Inc						D	4 111.241	
reman				1 7			Top of PVC Riser Elevat			atum: 111.34'	N7.4
oInsig	ht Eng	gineer/Geo	blogist: Jo	oshua E	Brown		Top of Protector Elevation	on: NS		round Elevation:	
					_		Date Started: 5/14/2021			ate Completed: 5	/14/2021
I	DRILI	LING ME	THOD			SAMPLER		GROUNDWATER M	<b>IEASUREMENTS</b>	5	
hicle: /	ATV				Type:	2" SS / Auto	Date	Depth (ft)	Reference	Stabiliz	ation
del: C	ME-8:	50			Hamn	ner (lb): 140	05/14/2021	24.64	Tan of Disco	1 hour	
thod:	Hollov	w stem aug	er		Fall (i	<b>n):</b> 30	05/23/2021	24.91	Top of Riser	9 da	ys
PTH	5	SAMPLE	INFORM	<b>IATIO</b>	N	WELL				FIELD	
(ft)		Pen/Rec	Depth			COMPLETION		IPLE	STRATUM	SCREENING	NOTI
_	#	(in)	(ft)	Blov	vs/6''	DETAIL	DESCR	IPTION	DESCRIPTION	(ppm)	
0 -		(111)	(11)		-		Switched to sampling even	w 10' due to time		(ppm)	
					-		constraints.	y to due to time			
1 -							constraints.				
2 -											
				-							
3 -				-							
, -				-			Cuttings: Material in cutting	ngs from 0-10' consistent			
				-			with other borings - Brown				
4 -				-			some gravel, damp.				
				-							
5 -				-							
					-						
6 -					-						
7 -											
										ļ	
8 -				-							
-											
9 -				-							
- 1					-						
.0 -				-					SAND &		
	S-1	24/12	10-12	1	7		S-1: Medium dense, brow	n, fine to coarse SAND,	GRAVEL	<1	1
1				1	3		some Gravel, trace Silt, da	mp			
1 -				1	3						
				1	2						
12 -				-							
				-	-						
3 -											
					-						
4 -					-						
-	<u> </u>			-							
				-	-						
6 -					-						
										ļ ļ	
7 -											
<u></u>				-							
8 -				-							
0				-							
0				-							
9 -				-							
				-							
- 0		GRAN	ULAR			COHESIVE	WELL				
		SO				SOILS	CONSTRUCTION	WELL	INTERVAL	LEGE	ND
	BI	lows/ft.	Dens	itv	Blows		NOTES	MATERIALS	(feet bgs)	LEGE	
		0-4	V. LO		<2		10110	Concrete	0-0.5		
		0-4 5-10	LOO		2-4				0-0.5		
								Backfill			
		11-30	M. DE		5-8		36' well constructed with	Grout	NA		
		31-50	DEN		9-15		3' standpipe and 33' bgs.	Bentonite: Chips	15-16		
		>50	V. DE	NSE	16-3		similar round bo ogs.	Sandpack: # 2 Sand	16-32		
					>30	HARD		Riser	22		
			1				I	Riser Screen	13		

-		<u> </u>	Client:	Bench	mark S	enior Living / Ti	ck Realty Corp.	Boring Identification	B-14 W	ell ID: GEO-6	
Geo	oIns	ighť				l (former Hector		Doring rechtmeation		<b>neet:</b> 2 of	r
		& Engineering				ad (Rt. 1), Rye		Chkd. By: DLS		roject Number: 9	
		nv: GeoS			elle K	Dad (Kl. 1), Kye		0310488 N 70.81242190 V		oject Number: 9	212
oreman		~	search, me	•			Top of PVC Riser Ele			atum: 111.34'	
		ineer/Geo	logiste Is	ahua D			Top of Protector Elev			round Elevation:	NIA
eomsig	gnt Eng	ineer/Get	Judgist: 10	isnua E	nown		Date Started: 5/14/202			ate Completed: 5	
		LING ME	THOD			SAMPLER	Date Started: 5/14/202		R MEASUREMENTS	<u> </u>	0/14/2021
		JING ME	THOD			2" SS / Auto	Dete			5 Stabiliz	- 4
ehicle:		-					Date 05/14/2021	Depth (ft)	Reference	1 ho	
Iodel: C						ner (lb): 140		24.64	Top of Riser		
		v stem aug				n): 30	05/23/2021	24.91		9 da	ys
DEPTH	2	AMPLE				WELL COMPLETIC	S.	MPLE	STRATUM	FIELD	NOTE
(ft)	#	Pen/Rec	-	Blov	vs/6''	DETAIL	DES	CRIPTION	DESCRIPTION	SCREENING (ppm)	NOIE
20 -	6.24	(in) 12/9	(ft) 20-21	1	8	DETAIL	C 14 Dance harmen G	AND the	SAND &	( <b>ppm</b> ) <1	1
	S-2A	12/9	20-21		6 6			ne to medium SAND, trace	GRAVEL	<1	1
21 -	S-2B	12/9	21.22		5		Silt, damp	AND and CUT 1-	OKAVEL	╂────┤	
	5-2B	12/9	21-22		3		5-20: Dense, brown, fi	ne SAND and SILT, damp		┣────┤	
22 -			$\vdash$		-					┝───┤	
	<u> </u>				-					<b>├</b> ──── <b>┤</b>	
23 -							Contines Weter at 271				
					-		Cutting: Water at ~25'				
24 -					-					<b>├</b> ──── <b>┤</b>	
					-					<b>├</b> ────┤	
25 -		0.1/2 /	05.55		-					<u>├</u>	
	S-3	24/24	25-27		5			ND and SILT, some Clay,		<1	1
26 -					5		wet			<b>├</b> ──── <b>┤</b>	
					5						
27 -					8				SAND & SILT		
					-						
28 -				-	-						
				-	-						
29 -				-	-						
				-	-						
30 -				-	-						
00				-	-					<1	1
31 -				-	-						
01				-	-						
32 -				-	-						
				-	-						
33 -				-	-			inated at 33' bgs.			
							Set monitor	ng well at 33' bgs			
34 -											
5-											
35 -											
55											
36											
36 -											
27											
37 -											
20											
38 -											
20											
39 -											
40											
40 -		GRAN	ULAR		(	COHESIVE	WELL				
			ILS			SOILS	CONSTRUCTION	WELL MATERIALS	INTERVAL (feat bgs)	LEGE	END
	Bl	ows/ft.	Dens	ity	Blows	/ft. Consistend		MATERIALS	(feet bgs)		
		0-4	V. LO	·	<2	V. SOFT		Concrete	0-0.5		
		5-10	LOO		2-4			Backfill	0.5-18		
		1-30	M. DE		5-8			Grout	NA		
		31-50	DEN		9-15		36' well constructed w	th Bentonite: Chine	18-19		
		>50	V. DEI		16-3		3' standpipe and 33' bg	s. Sandpack: # 2 Sand			
	1				>30			Riser	23		
	1					11111		Screen	13		
			1					bereen	10		

Soil samples screened in the field with a MiniRae 3000 photoionization detector with a 10.6 eV lamp.
 bgs = Below ground surface; NS = Not surveyed; WOH = Weight of hammer

# ATTACHMENT C

# LABORATORY ANALYTICAL REPORT

PROJECT9212-007 | June 17, 2021 NEW HAMPSHIRE | MASSACHUSETTS | CONNECTICUT | MAINE GEOINSIGHT.COM | INFO@GEOINSIGHT.COM | 800.271.1953

# Laboratory Report



124 Heritage Avenue Portsmouth NH 03801

Darrin Santos GeoInsight, Inc. 186 Granite Street 3rd Floor, Suite A Manchester, NH 03103



PO Number: None Job ID: 57095 Date Received: 5/24/21

Project: Benchmark Rye 9212-006

Attached please find results for the analysis of the samples received on the date referenced above.

Unless otherwise noted in the attached report, the analyses performed met the requirements of Absolute Resource Associates' Quality Assurance Plan. The Standard Operating Procedures are based upon USEPA SW-846, USEPA Methods for Chemical Analysis of Water and Wastewater, Standard Methods for the Examination of Water and Wastewater and other recognized methodologies. The results contained in this report pertain only to the samples as indicated on the chain of custody.

Absolute Resource Associates maintains certification with the agencies listed below. The reported results apply to the sample(s) in the condition as received at the time the laboratory took custody. This report shall not be reproduced except in full, without written approval of the laboratory. The liability of ARA is limited to the cost of the requested analyses, unless otherwise agreed upon in writing.

We appreciate the opportunity to provide laboratory services. If you have any questions regarding the enclosed report, please contact the laboratory and we will be glad to assist you.

Sincerely, Absolute Resource Associates

luer

Aaron DeWees Chief Operating Officer

Date of Approval: 6/1/2021 Total number of pages: 5

### Absolute Resource Associates Certifications

New Hampshire 1732 Maine NH902 Massachusetts M-NH902

Project ID: Benchmark Ry Job ID: 57095	ye 9212-006									
Sample#: 57095-001										
Sample ID: GEO-1										
Matrix: Water										
Sampled: 5/23/21 13	3:10	Reporting		Instr Dil'n		Prep		Anal	ysis	
Parameter	Result		Units	Factor	Analyst	Date	Batch	Date	Time	Reference
Ammonia as N	< 0.5	0.5	mg/L	1	SFM		2101459	5/25/21	9:40	SM4500NH3-
Chloride	220	2.5	mg/L	5	DBV		2101487	5/26/21	14:31	E300.0A
Nitrate-N	< 0.1	0.1	mg/L	1	DBV		2101441	5/24/21	12:37	E300.0A
Sample#: 57095-002										
Sample ID: GEO-2										
Matrix: Water										

<b>Sampled.</b> 0/20/21 10.20		Reporting		instr Dil'n		Prep		Anai	ysis	
Parameter	Result	Limit	Units	Factor	Analyst	Date	Batch	Date	Time	Reference
Ammonia as N	< 0.5	0.5	mg/L	1	SFM		2101459	5/25/21	9:40	SM4500NH3-D
Chloride	3.9	0.5	mg/L	1	DBV		2101487	5/26/21	15:20	E300.0A
Nitrate-N	2.2	0.1	mg/L	1	DBV		2101441	5/24/21	13:27	E300.0A

Sample#: 57095-003

Sample ID: GEO-3

Matrix: Water

Sampled: 5/23/21	13:30	Reporting		Instr Dil'n		Prep		Anal	ysis	
Parameter	Resu	ılt Limit	Units	Factor	Analyst	Date	Batch	Date	Time	Reference
Ammonia as N	< 0.	5 0.5	mg/L	1	SFM		2101459	5/25/21	9:40	SM4500NH3-D
Chloride	20	<b>0</b> 2.5	mg/L	5	DBV		2101487	5/26/21	14:47	E300.0A
Nitrate-N	1.	<b>1</b> 0.1	mg/L	1	DBV		2101441	5/24/21	13:43	E300.0A

Sample#: 57095-004

Sample ID: GEO-4

Matrix: Water

Sampled: 5/23/21	13:40		Reporting		Instr Dil'n		Prep		Anal	ysis	
Parameter		Result	Limit	Units	Factor	Analyst	Date	Batch	Date	Time	Reference
Ammonia as N		< 0.5	0.5	mg/L	1	SFM		2101459	5/25/21	9:40	SM4500NH3-D
Chloride		76	0.5	mg/L	1	DBV		2101487	5/26/21	15:37	E300.0A
Nitrate-N		1.4	0.1	mg/L	1	DBV		2101441	5/24/21	14:00	E300.0A

Sample#: 57095-005

Sample ID: GEO-5

Matrix: Water

Sampled: 5/23/21 13:50		Reporting		Instr Dil'n		Prep		Anal	ysis	
Parameter	Result	Limit	Units	Factor	Analyst	Date	Batch	Date	Time	Reference
Ammonia as N	0.9	0.5	mg/L	1	SFM		2101486	5/27/21	7:25	SM4500NH3-D
Chloride	12	0.5	mg/L	1	DBV		2101441	5/24/21	14:16	E300.0A
Nitrate-N	< 0.1	0.1	mg/L	1	DBV		2101441	5/24/21	14:16	E300.0A



Job ID: 57095

Sample#: 57095-006

Sample ID: GEO-6

Matrix: Water

Sampled: 5/23/21 14:00		Reporting		Instr Dil'n		Prep		Anal	ysis	
Parameter	Result	Limit	Units	Factor	Analyst	Date	Batch	Date	Time	Reference
Ammonia as N	< 0.5	0.5	mg/L	1	SFM		2101459	5/25/21	9:40	SM4500NH3-D
Chloride	240	2.5	mg/L	5	DBV		2101487	5/26/21	15:04	E300.0A
Nitrate-N	2.9	0.1	mg/L	1	DBV		2101441	5/24/21	14:33	E300.0A
Sample#: 57095-007										
Sample ID: MW-3										
Matrix: Water										
Sampled: 5/23/21 14:10		Reporting		Instr Dil'n		Prep		Anal	ysis	
Parameter	Result	Limit	Units	Factor	Analyst	Date	Batch	Date	Time	Reference
Ammonia as N	< 0.5	0.5	mg/L	1	SFM		2101459	5/25/21	9:40	SM4500NH3-D
Chloride	420	5.0	mg/L	10	DBV		2101487	5/26/21	13:58	E300.0A
Nitrate-N	1.3	0.1	mg/L	1	DBV		2101441	5/24/21	14:49	E300.0A
Sample#: 57095-008										
Sample ID: MW-6										
Matrix: Water										
Sampled: 5/23/21 14:20		Reporting		Instr Dil'n		Prep		Anal	ysis	
Parameter	Result	Limit	Units	Factor	Analyst	Date	Batch	Date	Time	Reference
Ammonia as N	< 0.5	0.5	mg/L	1	SFM		2101486	5/27/21	7:25	SM4500NH3-D
Chloride	430	5.0	mg/L	10	DBV		2101487	5/26/21	14:14	E300.0A
Nitrate-N	0.9	0.1	mg/L	1	DBV		2101441	5/24/21	15:05	E300.0A



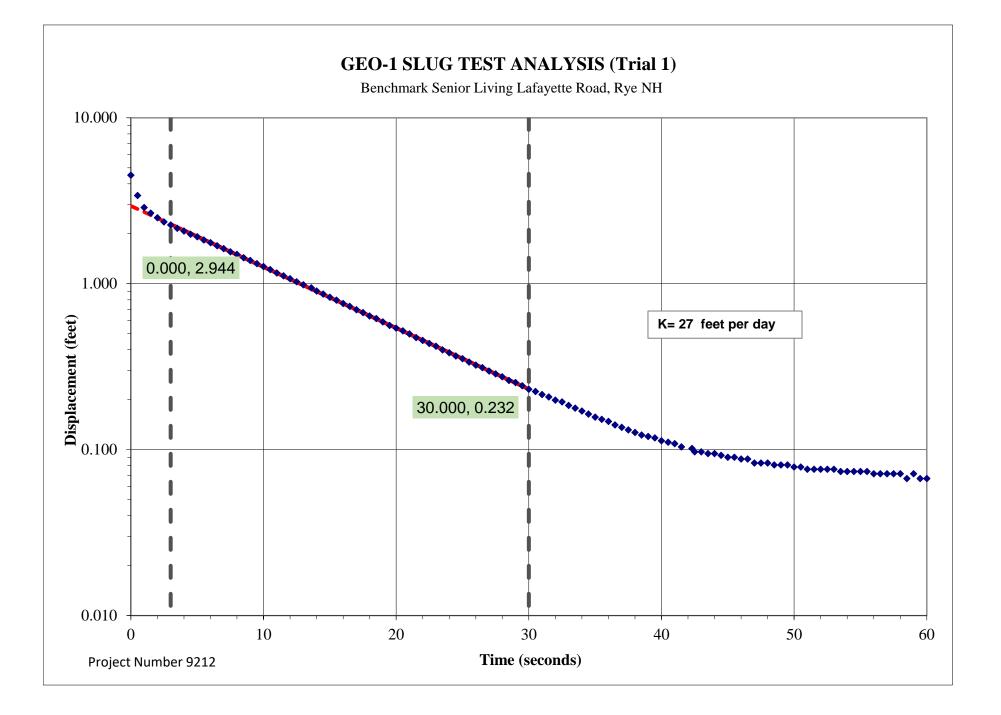
Abso	lute F	Resou	*		F	/				Port	smo 603	age Aver outh, NH -436-200	03801 )1							JST IS F	REC	วบ	ES	Т				and the second second	_	70	9		1 OF	
		socia	tes	C	9							1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1	ciates.co						-			AN	AL	YS	S	RE	QU	ES	r				-	
Company Name: Project Name: Re											2						11					ress			5		8			a-Nitrege				
Geo Insight Inc. Project #: 92																_						Hardness			Enterococci	nols	D Fluoride		Ð	NH.	1			
186 Granite St. Manchester NA							Project Location: NH MA ME VT										lechrin				it Colo			, ł		C L Ferrous I	D Phenois			esticio	4			
								Accreditation Required? N/Y:					MADEF	021VT	1	4	LIPH Hingerprint	8	noi		Color	□ Acidity	TAL Metals		-			D Bromide		CLP P	Loc			
Phone #: (Core) = 14 October Protocol:							otocol: RCRA SDWA NPDES MCP NHDES DOD				8260	UNC 8021VT	an	8	0	Pest/P	e dilu				TIC		1	N U N	Contho P	1000		dsh	Ammoni					
(605) 519-0820 Repo						Reporting QAPP GW-1 S-1					LI VOC 8260 MADEP		Dioxal	C Gas	NOEP	C 608.3 Pest/PCB	isotop		Turbidity	alinity	letais			LI Bacteria MPN		C Sulfate		SVOC	et A					
	Same	/	P. 1	2.5	1.1.1		-	Lir	Limits: EPA DW Other					1.1	SE, only	C 1,4-Dioxane	List			PFAS isotope dilution	664	in C	C Alkalinity	tant N		1		e + Ni			TCLP SVOC      TCLP Pesticide     Herbicides      Asbestos	S		
Email: DLSANTOS@ Geoinc.com						- Qu	Quote #						O NHD	EX MtB		01	a 14		33 🗆	Mineral 0&G 1664	ctivity	SVT D	C Priority Pollutant Metals		1 Boy	U U U IKN U Bacteria P/A	Nitrat	Chloride		0	-N trogan	0		
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ID (Lab Use Only)		D	# CONTAINERS	WATER	SOLID	OTHER	Ę	HNO	H <sub>2</sub> SO,	NaOH	MeOH	DATE	TIME	SAMPLER	C VOC 8260	D VOC 624.1	D VPH MADEP	C VOC 524.2	TPH 8100	0 8082 PCB	D PFAS 537,1	0&6 1664	HdD	D TSS	CRA Metals	Total Metals-list:	Dissolved Metals-list	T-Phosphorus	Cyanide	O Nitrate	Corrosivity	CLP Metals	Nitrak	in the second
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-05	GEO-	5	2	X					X				13:50																	X			X	
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Absolute Re	esource Associ		Sam	ple Recei	pt C	ondit	ion R	<i>eport</i> Job Number:	57095						
Samples Receiv			I-Fee	IEx D-USP	S	D-L	ab Cou		Drop-off -						
	- present & intac							CoC signed							
Receipt Temp:	- //	Samples or					J/A	-	24 hrs ago? -Yes -No						
neccipt remp.				ice? -Yes					of freezing? D-Yes D-No						
Comments:															
Preservation				Bottle Size/	Туре	& Qua	ntity		Check pH for ALL applicable*						
/ Analysis									samples and document:						
HCl	40mL(G)	250mL(P)		500mL(P)		1L(G)	_								
HNO <sub>3</sub>	125mL(P)	250mL(P)	_	500mL(P)		250-T	(P) 8	500mL(P)	AUZ SAM						
H <sub>2</sub> SO <sub>4</sub> NaOH	40mL(G) 125mL(P)	60mL(P) 250mL(P)	-	125mL(P)		250mL		SUUML(P)	forder						
(NH4)2SO4	60mL(P)	125mL(P)		250mL(P)			-		V						
ZnAc-NaOH	125mL(P)	250mL(P)													
Trizma	125mL(P)	250mL (P)	-						*pH ✓by analyst:VOC, PFAS, TOC,O&G Residual Cl not present:						
NH4Ac	125mL(P)	250mL (P)				-									
NaS <sub>2</sub> O <sub>3</sub>	40mL(G)	120mL(P)							ABN625Pest608						
MeOH	20mL(G)	40mL(G)	-	1					Bacteria ResCl ✓ by analyst						
None (solid)	2oz(G)	4oz(G)	-	8oz(G)		Syringe			PC Dry applicable? Y N						
None (water)	40ml (G)	60mL(P)	5	125mL(P)		250mL		500mL(P)	1L(G) 1L (P)						
rione (muter)			-												
Mold	Cassette	Bulk		Plate		Tape Lif									
Asbestos	Cassette	Bulk		Trate	-	Tape La									
Lead	Cassette	Bulk	-	Wipe											
	/					1									
							_								
Login Review	v				Yes	No	N/A	Comments							
Proper lab sam	ple containers/en	ough volume/co	orrect	preservative?	X										
Analyses marke	ed on COC match	bottles received	12		X	1									
	Vater-no headspace?						X	-							
VOC Solid-Met	OH covers solid, no	leaks, Prep Expira	tion C	DK?			~ ~								
PFAS: Lab spe	cific bottles? QC 1	received, if requi	red?				X								
Bacteria bottles	s provided by ARA	75			. /	-	X								
Samples within	holding time?				X	1									
	s communicated is	n writing:			X	0	21								
NO3 NO2,0-PO4,	pH, BOD, Coliform/I	E. coli (P/A or MPN)	), Ente	rococci, Color	C	34	DV .								
	lity, Odor, CrVI, Ferro		Dxygen	, Unpres 624	X										
	D on samples mat				2		x								
	inicated to analyst				-		1								
Subcontract no	ote on login board?	>													
Pesticides EPA	608 pH5-9?														
Compliance san	mples have no dise	crepancies/requi	ire no	flags?				(Or must be reject	ted)						
	sor notified imme						8		ppliance samples (NHDES, MADEP,						
Log-III Supervis	sor nounce mine	diately of follow	nig no	A	1			DoD etc.) or uncor	nmon requests.						
		d Received By:	_	R	n	_	Date,	/Time: 5/24	121 8:35						
Peer Review (	Checklist														
Client ID/I	Project Manager	🛛 On Ice, T	empe	rature OK?			Sample	e IDs	Analyses in Correctly						
D Project Nat	me	D PO# (if p	rovid	ed)			Matrix		-references						
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□ Received D		-		ove communic				HTs communicated							
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									OSD-04 Rev8 01/06/21 JVG (Page 1 of 1)						

# ATTACHMENT D

# SLUG TEST DATA AND HYDRAULIC CONDUCTIVITY CALCULATIONS

PROJECT 9212-007 | June 17, 2021 NEW HAMPSHIRE | MASSACHUSETTS | CONNECTICUT | MAINE GEOINSIGHT.COM | INFO@GEOINSIGHT.COM | 800.271.1953



Note L<sub>w</sub><H

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Instructions: enter values in shaded cells.

#### Well and Aquifer Parameters

Well casing diameter (2r <sub>c</sub> )	0.16667	feet
Boring diameter (2r <sub>w</sub> )	0.54167	feet
Height of water column in well $(L_w)$	13.07	feet
Length of saturated well screen ( $L_{\rm e}$ )	13.07	feet
Aquifer Thickness (H)	20	feet
Gravel pack porosity (n)	0.3	dimensionless
Anisotropy ratio (K <sub>r</sub> /K <sub>z</sub> )	10	dimensionless

Note:  $L_e$  will equal  $L_w$  for wells screened across the water table (shallow wells). Assumption Note: 30% porosity (0.3) is typical for gravel packs. Note: a value of 1 is equal to no anisotropy ( $K_z = K_p$ ).

Most sites will have an anisotropy ratio greater than 1 ( $K_r > K_z$ ).

#### Notes:

- 1. For a 2-inch diameter well, the well casing diameter (2r<sub>c</sub>) is 0.16667 feet and the boring diameter (2r<sub>w</sub>) is typically 0.54167 feet (6.5-inch diameter augers).
- 2. For a 4-inch diameter well, the well casing diameter  $(2r_c)$  is 0.33333 feet and the boring diameter  $(2r_w)$  is typically 0.6875 feet (8.25-inch diameter augers).
- 3. For a 6-inch diameter well, the well casing diameter  $(2r_c)$  is 0.5 feet and the boring diameter  $(2r_w)$  is typically 0.83333 feet (10-inch diameter augers).

Well casing radius (r <sub>c</sub> )	0.083335 feet	
Equivalent casing radius (r <sub>ce</sub> )	0.163911 feet	Note: corrected for porosity of gravel pack (shallow wells only).
Boring radius (r <sub>w</sub> )	0.270835 feet	
Corrected boring radius (r <sub>w</sub> *)	0.085646 feet	Note: corrected for anisotropy.
L <sub>e</sub> /r <sub>w</sub> (for Bouwer and Rice graph)	152.61 dimens	ionless

### Parameters from recovery graph

Displacement at t=0 (y <sub>0</sub> )	2.944 feet
Arbitrary time on straight line slope (t)	30.000 seconds
Displacement at that arbitrary time $(y_t)$	0.232 feet

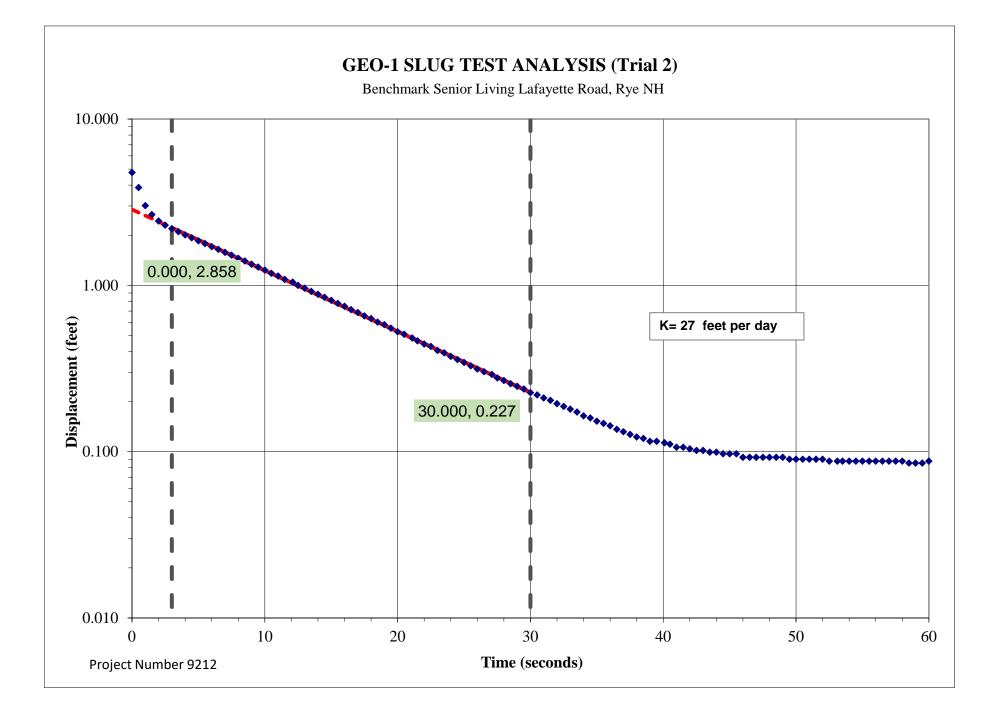
### Dimensionless Parameters (calculated from Bouwer and Rice Graph by linear interpolation)

A	5.39 dimensior	nless	
В	0.96 dimensior	hless	
Ln R <sub>e</sub> /r <sub>w</sub>	3.55014		
Hydraulic Conductivity (K)	3.09E-04 ft/sec	9.42E-03 cm/sec	2.67E+01 ft/day

#### References:

Bouwer, H. and Rice, R.C., 1976, A Slug Test for Determining Hydraulic Conductivity of Unconfined Aquifers With Completely or Partially Penetrating Wells. Water Resources Research, Vol. 12 No. 3, pp. 423-428.

Bouwer, H. 1989, The Bouwer and Rice Slug Test - An Update. Ground Water, Vol. 27, No. 3, pp. 304-309.



Note L<sub>w</sub><H

Benchmark Senior Living
Lafayette Road, Rye NH
9212
GEO-1
2

Instructions: enter values in shaded cells.

#### Well and Aquifer Parameters

Well casing diameter (2r <sub>c</sub> )	0.16667	feet
Boring diameter (2r <sub>w</sub> )	0.54167	feet
Height of water column in well $(L_w)$	13.07	feet
Length of saturated well screen ( $L_{\rm e}$ )	13.07	feet
Aquifer Thickness (H)	20	feet
Gravel pack porosity (n)	0.3	dimensionless
Anisotropy ratio (K <sub>r</sub> /K <sub>z</sub> )	10	dimensionless

Note:  $L_e$  will equal  $L_w$  for wells screened across the water table (shallow wells). Assumption Note: 30% porosity (0.3) is typical for gravel packs. Note: a value of 1 is equal to no anisotropy ( $K_z = K_p$ ).

Most sites will have an anisotropy ratio greater than 1 ( $K_r > K_z$ ).

Notes:

- 1. For a 2-inch diameter well, the well casing diameter (2r<sub>c</sub>) is 0.16667 feet and the boring diameter (2r<sub>w</sub>) is typically 0.54167 feet (6.5-inch diameter augers).
- 2. For a 4-inch diameter well, the well casing diameter  $(2r_c)$  is 0.33333 feet and the boring diameter  $(2r_w)$  is typically 0.6875 feet (8.25-inch diameter augers).
- 3. For a 6-inch diameter well, the well casing diameter  $(2r_c)$  is 0.5 feet and the boring diameter  $(2r_w)$  is typically 0.83333 feet (10-inch diameter augers).

Well casing radius (r <sub>c</sub> )	0.083335 feet	
Equivalent casing radius (r <sub>ce</sub> )	0.163911 feet	Note: corrected for porosity of gravel pack (shallow wells only).
Boring radius (r <sub>w</sub> )	0.270835 feet	
Corrected boring radius (r <sub>w</sub> *)	0.085646 feet	Note: corrected for anisotropy.
$L_e/r_w$ (for Bouwer and Rice graph)	152.61 dimensi	onless

### Parameters from recovery graph

Displacement at t=0 (y <sub>0</sub> )	2.858 feet
Arbitrary time on straight line slope (t)	30.000 seconds
Displacement at that arbitrary time $(y_t)$	0.227 feet

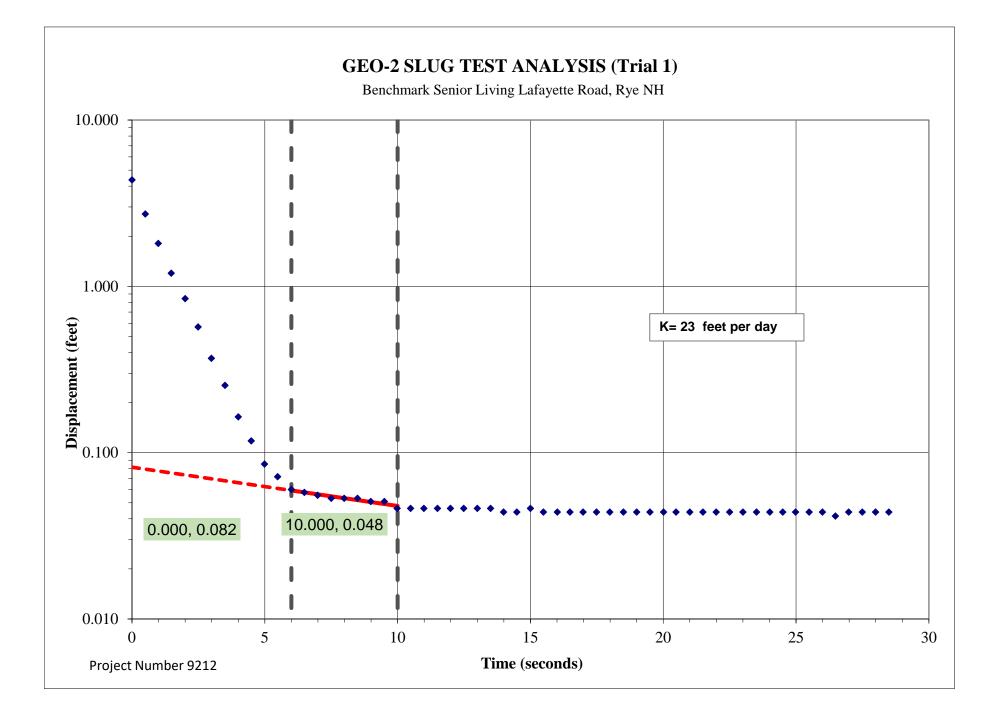
### Dimensionless Parameters (calculated from Bouwer and Rice Graph by linear interpolation)

А	5.39 dimension	less	
В	0.96 dimension	lless	
Ln R <sub>e</sub> /r <sub>w</sub>	3.55014		
Hydraulic Conductivity (K)	3.08E-04 ft/sec	9.39E-03 cm/sec	2.66E+01 ft/day

#### References:

Bouwer, H. and Rice, R.C., 1976, A Slug Test for Determining Hydraulic Conductivity of Unconfined Aquifers With Completely or Partially Penetrating Wells. Water Resources Research, Vol. 12 No. 3, pp. 423-428.

Bouwer, H. 1989, The Bouwer and Rice Slug Test - An Update. Ground Water, Vol. 27, No. 3, pp. 304-309.



Note L<sub>w</sub><H

Project Name:	Benchmark Senior Living
Project Address:	Lafayette Road, Rye NH
Project Number:	9212
Test Well:	GEO-2
Trial:	1

Instructions: enter values in shaded cells.

#### Well and Aquifer Parameters

Well casing diameter (2r <sub>c</sub> )	0.16667	feet
Boring diameter (2r <sub>w</sub> )	0.54167	feet
Height of water column in well $(L_w)$	8.39	feet
Length of saturated well screen $(L_e)$	8.39	feet
Aquifer Thickness (H)	20	feet
Gravel pack porosity (n)	0.3	dimensionless
Anisotropy ratio (K <sub>r</sub> /K <sub>z</sub> )	10	dimensionless

Note:  $L_e$  will equal  $L_w$  for wells screened across the water table (shallow wells). Assumption Note: 30% porosity (0.3) is typical for gravel packs. Note: a value of 1 is equal to no anisotropy ( $K_z = K_p$ ).

Most sites will have an anisotropy ratio greater than 1 ( $K_r > K_z$ ).

Notes:

- 1. For a 2-inch diameter well, the well casing diameter (2r<sub>c</sub>) is 0.16667 feet and the boring diameter (2r<sub>w</sub>) is typically 0.54167 feet (6.5-inch diameter augers).
- 2. For a 4-inch diameter well, the well casing diameter  $(2r_c)$  is 0.33333 feet and the boring diameter  $(2r_w)$  is typically 0.6875 feet (8.25-inch diameter augers).
- 3. For a 6-inch diameter well, the well casing diameter  $(2r_c)$  is 0.5 feet and the boring diameter  $(2r_w)$  is typically 0.83333 feet (10-inch diameter augers).

Well casing radius (r <sub>c</sub> )	0.083335 feet	
Equivalent casing radius (r <sub>ce</sub> )	0.163911 feet	Note: corrected for porosity of gravel pack (shallow wells only).
Boring radius (r <sub>w</sub> )	0.270835 feet	
Corrected boring radius (r <sub>w</sub> *)	0.085646 feet	Note: corrected for anisotropy.
$L_e/r_w$ (for Bouwer and Rice graph)	97.96 dimensi	onless

### Parameters from recovery graph

Displacement at t=0 (y <sub>0</sub> )	0.082 feet
Arbitrary time on straight line slope (t)	10.000 seconds
Displacement at that arbitrary time $(y_t)$	0.048 feet

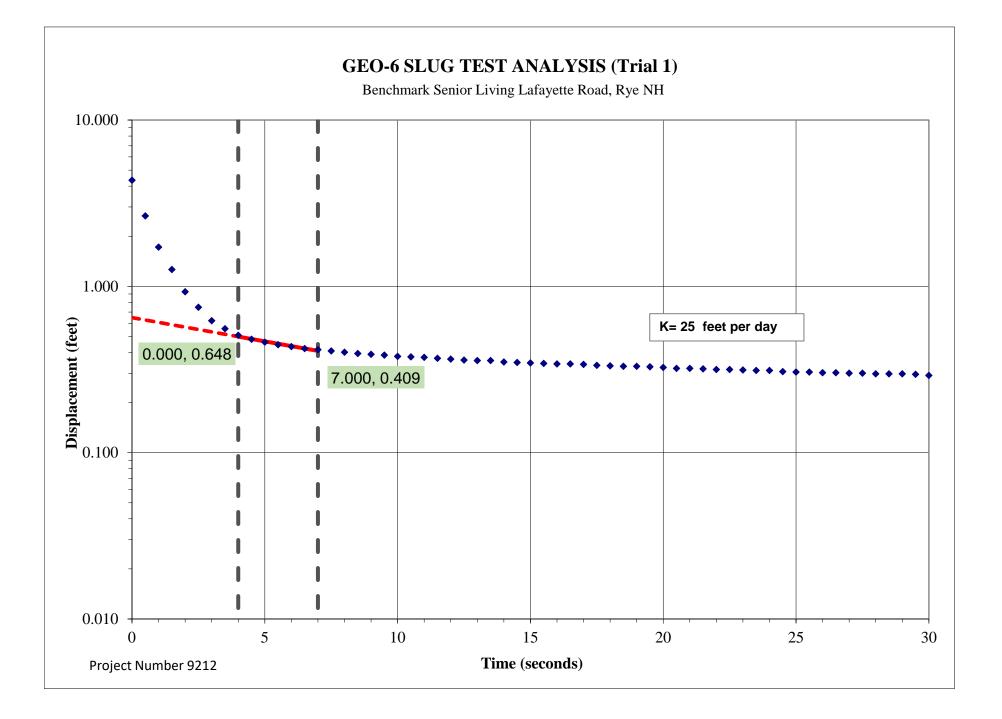
### Dimensionless Parameters (calculated from Bouwer and Rice Graph by linear interpolation)

A	4.31 dim	nensionless	
В	0.73 dim	nensionless	
Ln R <sub>e</sub> /r <sub>w</sub>	3.11975		
Hydraulic Conductivity (K)	2.68E-04 ft/s	sec 8.17E-03 cm/sec	2.32E+01 ft/day

#### References:

Bouwer, H. and Rice, R.C., 1976, A Slug Test for Determining Hydraulic Conductivity of Unconfined Aquifers With Completely or Partially Penetrating Wells. Water Resources Research, Vol. 12 No. 3, pp. 423-428.

Bouwer, H. 1989, The Bouwer and Rice Slug Test - An Update. Ground Water, Vol. 27, No. 3, pp. 304-309.



Note L<sub>w</sub><H

Project Name:	Benchmark Senior Living	
Project Address:	Lafayette Road, Rye NH	
Project Number:	9212	
Test Well:	GEO-6	
Trial:	1	

Instructions: enter values in shaded cells.

#### Well and Aquifer Parameters

Well casing diameter (2r <sub>c</sub> )	0.16667	feet
Boring diameter (2r <sub>w</sub> )	0.54167	feet
Height of water column in well $(L_w)$	10.19	feet
Length of saturated well screen (L $_{\rm e})$	10.19	feet
Aquifer Thickness (H)	20	feet
Gravel pack porosity (n)	0.3	dimensionless
Anisotropy ratio (K <sub>r</sub> /K <sub>z</sub> )	10	dimensionless

Note:  $L_e$  will equal  $L_w$  for wells screened across the water table (shallow wells). Assumption Note: 30% porosity (0.3) is typical for gravel packs. Note: a value of 1 is equal to no anisotropy ( $K_z = K_p$ ).

Most sites will have an anisotropy ratio greater than 1 ( $K_r > K_z$ ).

Notes:

- 1. For a 2-inch diameter well, the well casing diameter (2r<sub>c</sub>) is 0.16667 feet and the boring diameter (2r<sub>w</sub>) is typically 0.54167 feet (6.5-inch diameter augers).
- 2. For a 4-inch diameter well, the well casing diameter  $(2r_c)$  is 0.33333 feet and the boring diameter  $(2r_w)$  is typically 0.6875 feet (8.25-inch diameter augers).
- 3. For a 6-inch diameter well, the well casing diameter  $(2r_c)$  is 0.5 feet and the boring diameter  $(2r_w)$  is typically 0.83333 feet (10-inch diameter augers).

Well casing radius (r <sub>c</sub> )	0.083335 feet	
Equivalent casing radius (r <sub>ce</sub> )	0.163911 feet	Note: corrected for porosity of gravel pack (shallow wells only).
Boring radius (r <sub>w</sub> )	0.270835 feet	
Corrected boring radius (r <sub>w</sub> *)	0.085646 feet	Note: corrected for anisotropy.
L <sub>e</sub> /r <sub>w</sub> (for Bouwer and Rice graph)	118.98 dimensio	nless

### Parameters from recovery graph

Displacement at t=0 ( $y_0$ )	0.648 feet
Arbitrary time on straight line slope (t)	7.000 seconds
Displacement at that arbitrary time $(y_t)$	0.409 feet

### Dimensionless Parameters (calculated from Bouwer and Rice Graph by linear interpolation)

Α	4.74 dimensior	nless	
В	0.82 dimensionless		
Ln R <sub>e</sub> /r <sub>w</sub>	3.30422		
Hydraulic Conductivity (K)	2.86E-04 ft/sec	8.72E-03 cm/sec	2.47E+01 ft/day

#### References:

Bouwer, H. and Rice, R.C., 1976, A Slug Test for Determining Hydraulic Conductivity of Unconfined Aquifers With Completely or Partially Penetrating Wells. Water Resources Research, Vol. 12 No. 3, pp. 423-428.

Bouwer, H. 1989, The Bouwer and Rice Slug Test - An Update. Ground Water, Vol. 27, No. 3, pp. 304-309.

# ATTACHMENT E

# COAKLEY LANDFILL INFORMATION

PROJECT9212-007 | June 17, 2021 NEW HAMPSHIRE | MASSACHUSETTS | CONNECTICUT | MAINE GEOINSIGHT.COM | INFO@GEOINSIGHT.COM | 800.271.1953 2014 FEB 27 PM 12: 11

ROCKINGHAM COUNTY REGISTRY OF DEEDS

# NOTICE OF GROUNDWATER MANAGEMENT PERMIT GWP-198712001-N-002 TO BE RECORDED AGAINST:

### Coakley Landfill Inc. Bk1340 P254 and Bk1347 P172

NOTICE IS HEREBY GIVEN THAT: The New Hampshire Department of Environmental Services (Department) has issued Groundwater Management Permit #GWP-198712001-N-002 ("Permit") to the Coakley Landfill Group. Pursuant to Env-Or 607.09(a) this notice is recorded for each property located within the groundwater management zone identified in the Permit at the Registry of Deeds in Rockingham County.

The Permit establishes a Groundwater Management Zone ("GMZ"), an area within which groundwater use must be controlled and monitored due to the presence of groundwater contaminants that exceed the State's Ambient Groundwater Quality Standards ("AGQS"). The Permit may include conditions to and restrictions upon the use of the properties within the GMZ, including restrictions on the use of groundwater.

The Permit was originally issued on June 19, 2008 and renewed January 7, 2014 expires on January 6, 2019, unless renewed for subsequent five-year period(s). This Notice will remain in effect until such time as the AGQS are restored within the GMZ and the Department issues a Release of Recordation to the Permittee. The Permit is available for review at the New Hampshire Department of Environmental Services, 29 Hazen Drive, Concord, NH 03301 or viewed bv searching under our OneStop Data Retrieval can be Site at http://www2.des.nh.gov/OneStop/ORCB Query.aspx?Project+CCST.

The following properties are located within the GMZ:

Tax Map / Lot No.	Property Address	Owner	Deed Ref. (Book / Page)
6/37	365 Lafayette Road, Rye	SNS LLC	5238/2463
10/11	355 Lafayette Road, Rye	Malcolm E. Smith III	5079/0262
17/72	67 North Road, North Hampton	Joan M Nordstrom	2416/583
17/73	65 North Road, North Hampton	Joseph F and Yolanda Fitzgerald	3007/2807
17/82	160 Lafayette Road, North Hampton	Luck Enterprises, Inc.	2473/1659
17/86	180 Lafayette Road, North Hampton	Christopher C and Louis J Fucci	3319/952
17/87	186 Lafayette Road, North Hampton	Lori A Lessard Trustee	2760/2099
21/8	188 Lafayette Road, North Hampton	Joseph J and Helen M McKittrick	2641/2656
21/10	8A Lafayette Terrace, North Hampton	John J Sr and Dorleena Wylie	4030/2567
21/11	12A Lafayette Terrace, North Hampton	Seth McAlister	5044/102
21/12	16A Lafayette Terrace, North Hampton	William and Christine Adinolfo	2963/1721
21/14	20 Lafayette Terrace, North Hampton	Joseph Hanley	4682/1265
21/14-1	40-42 Lafayette Terrace, North Hampton	James A C Jones	4451/1104
21/15	44 Lafayette Terrace, North Hampton	Joseph B and Bridget S Conner	4183/1638
21/16	46 Lafayette Terrace, North Hampton	Rodney K Booker Trustee	5196/2724
21/17	1 Lafayette Terrace, North Hampton	Judith I and Bernard P Tracey	2450/687

21/18	3 Lafayette Terrace, North	Erin and Joshua Miller	5029/1768
21/19	Hampton 5 Lafayette Terrace, North Hampton	Richard P and Kimberly M Bartlett	3824/2799
21/20	9 Lafayette Terrace, North Hampton	Alexis J Perron III	3088/1774
21/21	11 Lafayette Terrace, North Hampton	Kenneth and Tracey Margeson	3121/1606
21/22	15 Lafayette Terrace, North Hampton	Edward and Anita Gabree	3013/2221
21/23	Part of 11 Lafayette Terrace	Kenneth and Tracey Margeson	3121/1606
21/24	43 Lafayette Terrace, North Hampton	William Warman	4374/1365
21/25	45 Lafayette Terrace, North Hampton	ZCCMMXIIVOOOOOIIIII5INH LTD Partnership	2530/1863
21/26	198 Lafayette Road, North Hampton	Gozinta LLC	4275/904
21/27	206 Lafayette Road, North Hampton	206 Lafayette Road LLC	4785/379
21/27-1	200 Lafayette Road, North Hampton	Derek R Burt Trustee	5147/325
21/28	216 Lafayette Road, North Hampton	Stella A Ciborowski Trust	2414/729
21/28-1	216 Lafayette Road, North Hampton	Leo J Crotty Jr	2475/1278
21/29	212 Lafayette Road, North Hampton	S&L Realty Trust	3666/1199
21/31	224 Lafayette Road, North Hampton	SNS LLC	5238/2463
21/32	Coakley Landfill, North Hampton	Coakley Landfill LLC	3117/2934
21/33	Coakley Landfill, North Hampton	Coakley Landfill LLC	3117/2934
21/34	Lafayette Road Rear, North Hampton	James A C Jones	4451/1102

21/35	Lafayette Terrace Rear, North Hampton	James A C Jones	4451/1102
21/36	Lafayette Terrace Rear, North Hampton	James A C Jones	4451/1102
21/37	Lafayette Terrace Rear, North Hampton	Town of North Hampton	3415/1661
21/39	North Road Rear, North Hampton	Joan, Breen and Denise Grenier- Winther, Susan Sherr, and Caryn Blake	5142/2979
21/41	North Road Rear, North Hampton	Elmer M Sewall	1340/524
21/46	10 Lafayette Terrace / Part of 8A, North Hampton	John J Sr and Dorleena L Wylie	3219/2588
*R1/13	340 Breakfast Hill Road (Portion Only)	Elmer M Sewall Rev Trust 96	3159/928
R1/9B	560 Breakfast Hill Road	Town of Greenland	3454/1131

Shaded rows indicate newly added lots.

\*An expanded portion of the Sewall parcel (Tax Map R1 Lot #13) is included within the GMZ, as shown on the updated plot plan entitled "*Groundwater Monitoring Zone Plan*" prepared by Richard D. Bartlett & Associates, LLC., certified on December 11, 2013, and described as follows:

Commencing at a point on the easterly line of land now or formerly of the Boston and Maine Corporation, said point being a distance of 600.93 feet as measured along a curve to the left, having a central angle of 01°54'46" and a radius of 18,000.00 feet, from a steel pin set on the southerly sideline of Breakfast Hill Road marking the northeasterly most corner of said Boston and Maine land identified on tax map R1 as lot 11, thence by a curve to the left, having a central angle of 00°33'15" and a radius of 18,000.00 feet, a distance of 174.06 feet to a point, thence by a curve to the left, having a central angle of 00°24'32" and a radius of 11,425.51 feet, a distance of 81.56 feet to a point; thence S13º08'30"W a distance of 1,419.54 feet to a point; thence, N76°51'30"W a distance of 99.00 feet to a point at land now or formerly of Elmer M. Sewall Revocable Trust 96, thence, along said Sewall land, N35º09'35"E a distance of 88.02 feet to a point; thence, continuing by said Sewall land, N13º08'30"E a distance of 163.21 feet to a point; thence N76º51'30"W a distance of 434.00 feet, through said Sewall land to a point; thence S17°29'30"W a distance of 1,097.80 feet to a point on the Greenland-North Hampton town line, said point being N79°55'00"W a distance of 18.99 feet from a concrete bound, on said town line. engraved "G" and "N-H", thence, along said town line, N79°55'00"W a distance of 345.00 feet to a point; thence N23°21'55"E a distance of 2,504.63 feet to a point; thence N25°28'15"E a distance of 551.47 feet to a point; thence S72°51'15"E a distance of 221.87 feet to a point; thence S15°37'10"W a distance of 441.43 feet to a point; thence S75°34'35"E a distance of 166.70 feet continuing through said Sewall land and said

Boston and Maine land to the point of beginning.

Containing 1,306,532 square feet or 29.99 acres, of which 27.42 acres is the land of the Elmer M. Sewall Revocable Trust 96 and 2.57 acres is the land of the Boston and Maine Corporation.

G February 26, 2014

/s/Robert Sullivan, Permittee Coakley Landfill Group

Approved pursuant to authorization of Coakley Executive Committee via electronic communication



The

# NEW HAMPSHIRE DEPARTMENT OF ENVIRONMENTAL SERVICES

## hereby issues

## GROUNDWATER MANAGEMENT PERMIT NO. GWP-198712001-N-002

to the permittee

# COAKLEY LANDFILL GROUP

## to monitor the past discharge of

Contaminants Of Concern (as identified in Table 12 of the 1994 Record of Decision and subsequent decision documents)

at

## COAKLEY LANDFILL (480 Breakfast Hill Road)

## in NORTH HAMPTON, N.H.

via the groundwater, surface water and sediment monitoring system comprised of

32 monitoring wells, 3 surface water, 2 sediment, and 1 leachate sampling locations and 5 residential drinking water supply wells

as depicted on the Site Plan and tables entitled

Environmental Monitoring Network (site plan); OU-1 Groundwater Monitoring Wells and Water Supply Wells; and OU-2 Groundwater Monitoring Wells

dated September 2013 (site plan) and July 2013 Revision 2.0 (tables), prepared by Summit Environmental Consultants

TO: COAKLEY LANDFILL GROUP 1 JUNKINS AVENUE PORTSMOUTH, NEW HAMPSHIRE 03801

Date of Issuance: January 7, 2014 Date of Expiration: January 6, 2019

(continued)

Pursuant to authority in N.H. RSA 485-C:6-a, the New Hampshire Department of Environmental Services (Department), hereby grants this permit to monitor past discharges to the groundwater at the above described location for five years subject to the following conditions:

## STANDARD MANAGEMENT PERMIT CONDITIONS

- 1. The permittee shall not violate Ambient Groundwater Quality Standards adopted by the Department (N.H. Admin. Rules Env-Or 600) in groundwater outside the boundaries of the Groundwater Management Zone, as shown on the referenced site plan and updated on the plot plan entitled "*Groundwater Monitoring Zone Plan*" prepared by Richard D. Bartlett & Associates, LLC., certified on December 11, 2013.
- 2. The permittee shall not cause groundwater degradation that results in a violation of surface water quality standards (N.H. Admin. Rules Env-Ws 1700) in any surface water body.
- 3. The permittee shall allow any authorized staff of the Department, or its agent, to enter the property covered by this permit for the purpose of collecting information, examining records, collecting samples, or undertaking other action associated with this permit.
- 4. The permittee shall apply for the renewal of this permit at least 90 days prior to its expiration date.
- 5. This permit is transferable only upon written request to, and approval of, the Department. Compliance with the existing Permit shall be established prior to permit transfer. Transfer requests shall include the name and address of the person to whom the permit transfer is requested, signature of the current and future permittee, and a summary of all monitoring results to date.
- 6. The Department reserves the right, under N.H. Admin. Rules Env-Or 600, to require additional hydrogeologic studies and/or remedial measures if the Department receives information indicating the need for such work.
- 7. The permittee shall maintain a water quality monitoring program and submit monitoring results to the Department's Waste Management Division no later than 45 days after sampling. Samples shall be taken from site monitoring wells, surface water and sediment sampling points as shown and labeled on the referenced site plan in accordance with the schedule outlined herein:

Monitoring Locations	Sampling Frequency	Parameters
FPC-4B, AE-4B	August each year	Bedrock well - field parameters, TAL metals (total, unless highly turbid), NHDES Waste Management Division full list of analytes for volatile organics (full list VOCs).
FPC-5A, MW-4, MW-9, OP-2	August each year	Overburden wells – field parameters, TAL metals ( <u>dissolved</u> ), 1,4-dioxane.
FPC-6B, FPC-8B, GZ- 105, AE-2B, AE-3B, MW-5S, MW-5D, MW-6, MW-8, MW-11	August each year	Bedrock wells – field parameters, TAL metals (t <b>otal, unless highly turbid</b> ), full list VOCs, 1,4-dioxane.
FPC-7A, FPC-9A, FPC- 11A, AE-1A, MW-10, OP-5	August each year	Overburden wells – field parameters, TAL metals ( <u>dissolved</u> )

- 3 -Monitoring Locations	Sampling Frequency	Parameters			
FPC-5B, BP-4	August each year	Bedrock well – field parameters, TAL metals (total, unless highly turbid), 1,4-dioxane.			
FPC-6A, FPC-8A, AE-2A, AE-3A	August each year	Overburden wells – field parameters, TAL metals ( <u>dissolved</u> ), full list VOCs, 1,4- dioxane.			
AE-4A	August each year	Overburden well – field parameters, TAL metals ( <b>dissolved</b> ), full list VOCs.			
FPC-7B, FPC-11B, AE-1B	August each year	Bedrock wells – field parameters, TAL metals ( <u>total, unless highly turbid</u> ).			
Residential, Surface Water, Sediment & Leachate					
368BHR (R-3), 339BHR	August & February each year	Bedrock drinking water well – Field parameters, arsenic & manganese ( <u>total</u> ), VOCs full list (EPA Method 524), 1,4-dioxane.			
399BHR (R-5), 346BHR, 415BHR	August each year	Field parameters, arsenic & manganese ( <u>total</u> ), NHDES full list (EPA Method 524), 1,4-dioxane.			
SW-4, SW-5, SW-103 August each year		Field parameters, ammonia, TAL metals (dissolved), full list VOCs.			
SED-4, SED-5	August each year	Metals (total).			
L-1	August each year	Field parameters, COD, ammonia, TAL metals ( <b>dissolved</b> ).			

Sampling shall be performed in accordance with the documents listed in Env-Or 610.02 (e) and the approved Environmental Monitoring Plan. Samples shall be analyzed by a laboratory certified by the U.S. Environmental Protection Agency or the New Hampshire Department of Environmental Services pursuant to Env-C 300. All overburden groundwater samples collected for metal analyses shall be analyzed for dissolved metals; and thus must be field filtered (with a 0.45-micron filter) and acidified after filtration in the field. Surface water samples and samples collected from bedrock or water supply wells shall be analyzed for total metals, and shall not be filtered. As referred to herein, the term "TAL Metals" refers to aluminum, arsenic, barium, cadmium, calcium, chromium, copper, iron, lead, magnesium, mercury, nickel, potassium, selenium, silver, sodium, thallium, zinc, cobalt, beryllium, manganese, antimony, and vanadium.

Summaries of water quality shall be submitted annually to the Department's Waste Management Division, in the month of February, using a format acceptable to the Department. The Summary Report shall include the information listed in Env-Or 607.04 (a), as applicable.

The Annual Summary Report shall be prepared and stamped by a professional engineer or professional geologist licensed in the State of New Hampshire.

- Issuance of this permit is based on the Groundwater Management Permit Application dated October 3, 2013 and the historical documents found in the Department file DES #198712001. The Department may require additional hydrogeologic studies and/or remedial measures if invalid or inaccurate data are submitted.
- 9. Within 15 days of the date of Department approval of this Groundwater Management Permit, the permittee shall provide notice of the permit by certified mail, return receipt requested, to all owners of **newly added lots** of record (i.e., not noticed under original permit) within the Groundwater Management Zone (see shaded lots in Special Condition #12). The permittee shall submit documentation of this notification to the Department within 45 days of permit issuance.

(continued)

- 10. Within 60 days of the date of Department approval of this Groundwater Management Permit, the permit holder shall record notice of the permit in the registry of deeds in the chain of title for each **newly added lot** within the Groundwater Management Zone (see shaded lots in Special Condition #12). The original notice on Lot 13 Map R1 shall be amended to reflect the expanded GMZ within this lot. **Recordation requires that the registry be provided with the name of current property owner and associated book and page numbers for the deed of each lot encumbered by this permit. Portions of State/Town/City roadways and associated right-of-way properties within the Groundwater Management Zone do not require recordation.** A copy of each recorded notice shall be submitted to the Department and to the governing body of each municipality in which the site or any lot within the GMZ is located within 30 days of recordation.
- 11. Within 30 days of discovery of a violation of an ambient groundwater quality standard at or beyond the Groundwater Management Zone boundary, the permittee shall notify the Department in writing. Within 60 days of discovery, the permittee shall submit recommendations to correct the violation. The Department shall approve the recommendations if the Department determines that they will correct the violation.

## SPECIAL CONDITIONS FOR THIS PERMIT

12. Recorded property within the Groundwater Management Zone shall include the lots, or portions thereof, as listed and described in the following table:

Tax Map / Lot No.	Property Address	Owner	Deed Ref. (Book / Page)
6/37	365 Lafayette Road, Rye	SNS LLC	5238/2463
10/11	355 Lafayette Road, Rye	Malcolm E. Smith III	5079/0262
17/72	67 North Road, North Hampton	Joan M Nordstrom	2416/583
17/73	65 North Road, North Hampton	Joseph F and Yolanda Fitzgerald	3007/2807
17/82	160 Lafayette Road, North Hampton	Luck Enterprises, Inc.	2473/1659
17/86	180 Lafayette Road, North Hampton	Christopher C and Louis J Fucci	3319/952
17/87	186 Lafayette Road, North Hampton	Lori A Lessard Trustee	2760/2099
21/8	188 Lafayette Road, North Hampton	Joseph J and Helen M McKittrick	2641/2656
21/10	8A Lafayette Terrace, North Hampton	John J Sr and Dorleena Wylie	4030/2567
21/11	12A Lafayette Terrace, North Hampton	Seth McAlister	5044/102
21/12	16A Lafayette Terrace, North Hampton	William and Christine Adinolfo	2963/1721
21/14	20 Lafayette Terrace, North Hampton	Joseph Hanley	4682/1265
21/14-1	40-42 Lafayette Terrace, North Hampton	James A C Jones	4451/1104
21/15	44 Lafayette Terrace, North Hampton	Joseph B and Bridget S Conner	4183/1638
21/16	46 Lafayette Terrace, North Hampton	Rodney K Booker Trustee	5196/2724

Tax Map / Lot No.	Property Address	Owner	Deed Ref. (Book / Page)	
21/17	1 Lafayette Terrace, North Hampton	Judith I and Bernard P Tracey	2450/687	
21/18	3 Lafayette Terrace, North Hampton	Erin and Joshua Miller	5029/1768	
21/19	5 Lafayette Terrace, North Hampton	Richard P and Kimberly M Bartlett	3824/2799	
21/20	9 Lafayette Terrace, North Hampton	Alexis J Perron III	3088/1774	
21/21	11 Lafayette Terrace, North Hampton	Kenneth and Tracey Margeson	3121/1606	
21/22	15 Lafayette Terrace, North Hampton	Edward and Anita Gabree	3013/2221	
21/23	Part of 11 Lafayette Terrace	Kenneth and Tracey Margeson	3121/1606	
21/24	43 Lafayette Terrace, North Hampton	William Warman	4374/1365	
21/25	45 Lafayette Terrace, North Hampton	ZCCMMXIIVOOOOOIIIII5INH LTD Partnership	2530/1863	
21/26	198 Lafayette Road, North Hampton	Gozinta LLC	4275/904	
21/27	206 Lafayette Road, North Hampton	206 Lafayette Road LLC	4785/379	
21/27-1	200 Lafayette Road, North Hampton	Derek R Burt Trustee	5147/325	
21/28	216 Lafayette Road, North Hampton	Stella A Ciborowski Trust	2414/729	
21/28-1	216 Lafayette Road, North Hampton	Leo J Crotty Jr	2475/1278	
21/29	212 Lafayette Road, North Hampton	S&L Realty Trust	3666/1199	
21/31	224 Lafayette Road, North Hampton	SNS LLC	5238/2463	
21/32	Coakley Landfill, North Hampton	Coakley Landfill LLC	3117/2934	
21/33	Coakley Landfill, North Hampton	Coakley Landfill LLC	3117/2934	
21/34	Lafayette Road Rear, North Hampton	James A C Jones	4451/1102	
21/35	Lafayette Terrace Rear, North Hampton	James A C Jones	4451/1102	
21/36	Lafayette Terrace Rear, North Hampton	James A C Jones	4451/1102	
21/37	Lafayette Terrace Rear, North Hampton	Town of North Hampton	3415/1661	
21/39	North Road Rear, North Hampton	Joan, Breen and Denise Grenier- Winther, Susan Sherr, and Caryn Blake	5142/2979	
21/41	North Road Rear, North Hampton	Elmer M Sewall	1340/524	
21/46	10 Lafayette Terrace / Part of 8A, North Hampton	John J Sr and Dorleena L Wylie	3219/2588	

- 5 -

Tax Map / Lot No.	Property Address	Owner	Deed Ref. (Book / Page)
*R1/13	340 Breakfast Hill Road (Portion Only)	Elmer M Sewall Rev Trust 96	3159/928
R1/9B	560 Breakfast Hill Road	Town of Greenland	3454/1131

Shaded rows indicate newly added lots that require notice per Standard Permit Conditions #9 and #10. The original notice on Lot 13 Map R1 should be amended and recorded to reflect the expanded GMZ within this lot.

\*An expanded portion of the Sewall parcel (Tax Map R1 Lot #13) is included within the GMZ, as shown on the updated plot plan entitled "*Groundwater Monitoring Zone Plan*" prepared by Richard D. Bartlett & Associates, LLC., certified on December 11, 2013, and described as follows:

Commencing at a point on the easterly line of land now or formerly of the Boston and Maine Corporation, said point being a distance of 600.93 feet as measured along a curve to the left, having a central angle of 01°54'46" and a radius of 18,000.00 feet, from a steel pin set on the southerly sideline of Breakfast Hill Road marking the northeasterly most corner of said Boston and Maine land identified on tax map R1 as lot 11, thence by a curve to the left, having a central angle of 00°33'15" and a radius of 18,000.00 feet, a distance of 174.06 feet to a point, thence by a curve to the left, having a central angle of 00°24'32" and a radius of 11,425.51 feet, a distance of 81.56 feet to a point; thence S13°08'30"W a distance of 1,419.54 feet to a point; thence, N76°51'30"W a distance of 99.00 feet to a point at land now or formerly of Elmer M. Sewall Revocable Trust 96, thence, along said Sewall land, N35°09'35"E a distance of 88.02 feet to a point; thence, continuing by said Sewall land, N13º08'30"E a distance of 163.21 feet to a point; thence N76º51'30"W a distance of 434.00 feet, through said Sewall land to a point; thence S17°29'30"W a distance of 1,097.80 feet to a point on the Greenland-North Hampton town line, said point being N79°55'00"W a distance of 18.99 feet from a concrete bound, on said town line, engraved "G" and "N-H", thence, along said town line, N79°55'00"W a distance of 345.00 feet to a point; thence N23°21'55"E a distance of 2,504.63 feet to a point; thence N25°28'15"E a distance of 551.47 feet to a point; thence S72°51'15"E a distance of 221.87 feet to a point; thence S15°37'10"W a distance of 441.43 feet to a point; thence S75°34'35"E a distance of 166.70 feet continuing through said Sewall land and said Boston and Maine land to the point of beginning.

Containing 1,306,532 square feet or 29.99 acres, of which 27.42 acres is the land of the Elmer M. Sewall Revocable Trust 96 and 2.57 acres is the land of the Boston and Maine Corporation.

## 13. INSTALLATION OF NEW GMZ COMPLIANCE WELLS

Two well couplets (overburden and bedrock) shall be installed near the revised GMZ boundary. Locations to be confirmed with EPA & DES prior to construction. Wells shall be installed and sampled as part of the regular scheduled 2014 sampling program.

## 14. <u>UNDEVELOPED LOTS WITHIN THE GROUNDWATER MANAGEMENT ZONE</u>:

Consistent with Env-Or 607.06(d), for each undeveloped lot, or portion thereof, which is within the Groundwater Management Zone and lacks access to a public water supply, the permittee shall contact the property owner annually to determine if a water supply well has been installed. The permittee shall include a report on this inquiry in the Annual Summary Report required in Standard Permit Condition #7. The results of these inquiries shall be documented in each Annual Summary Report.

Upon discovery of a new drinking water supply well within the Groundwater Management Zone, the permittee shall provide written notification to the Department and, to ensure compliance with Env-Or 607.06(a), submit a contingency plan to provide potable drinking water in the event the well is or becomes contaminated above the ambient groundwater quality standards. The potable water supply shall meet applicable federal and state water quality criteria. This plan shall be submitted to the Department for approval within 15 days of the date of discovery.

The permittee shall sample the new supply well within 30 days of discovery. The well shall be sampled for all the analytical parameters included in Standard Condition # 7, unless otherwise specified in writing by the Department. The permittee shall forward all analytical results to the Department's Waste Management Division, the Department's Environmental Health Program, and the owner of the drinking water supply well within 7 days of receipt of the results.

If the results for the new well meet the ambient groundwater quality standards, the permittee shall continue to sample the new wells annually as part of the permit. If the results for the new well indicate a violation of the ambient groundwater quality standards, the permittee shall notify the owner immediately and conduct confirmatory sampling within 14 days of receiving the original results.

Upon confirmation of a violation of the ambient groundwater quality standards in a new drinking water well, the permittee shall immediately implement the contingency plan to provide a potable drinking water supply that meets applicable federal and state water quality criteria.

- 15. All monitoring wells at the site shall be properly maintained and secured from unauthorized access or surface water infiltration.
- 16. The permittee shall update ownership information required by Env-Or 607.03(a)(20) for all properties within the Groundwater Management Zone prior to renewal of the permit or upon a recommendation for site closure.

IN. Bast

Carl W. Baxter, P.E., Administrator Hazardous Waste Remediation Bureau Waste Management Division

Under RSA 21-0:14 and 21-0:9-V, any person aggrieved by any terms or conditions of this permit may appeal to the Waste Management Council in accordance with RSA 541-A and N.H. Admin. Rules, Env-WMC 200. Such appeal must be made to the Council within 30 days and must be addressed to the Chairman of the Waste Management Council, c/o Appeals Clerk, Department of Environmental Services Legal Unit, 29 Hazen Drive, P.O. Box 95, Concord, NH 03302-0095.

GWP-198712001-N-002

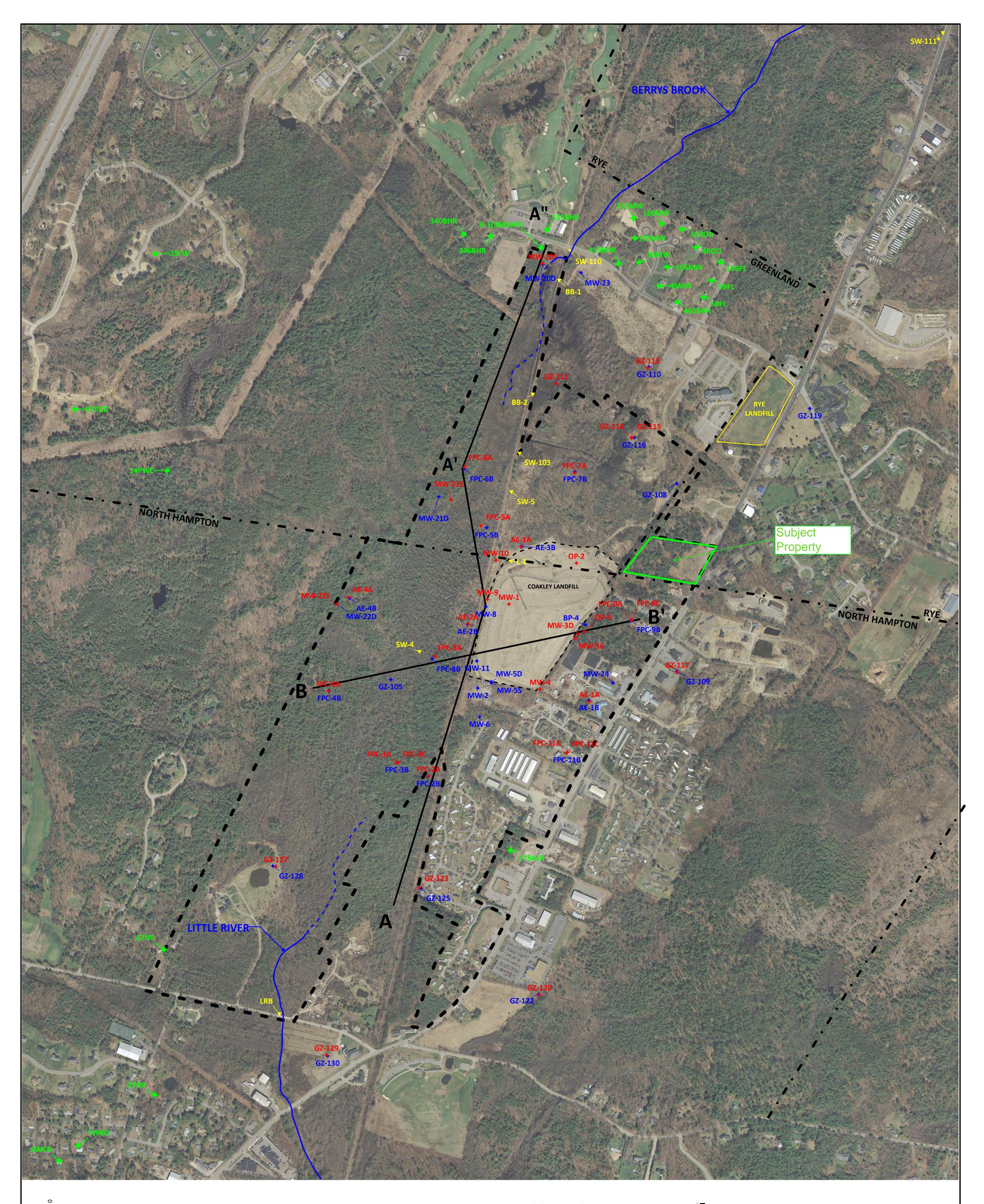
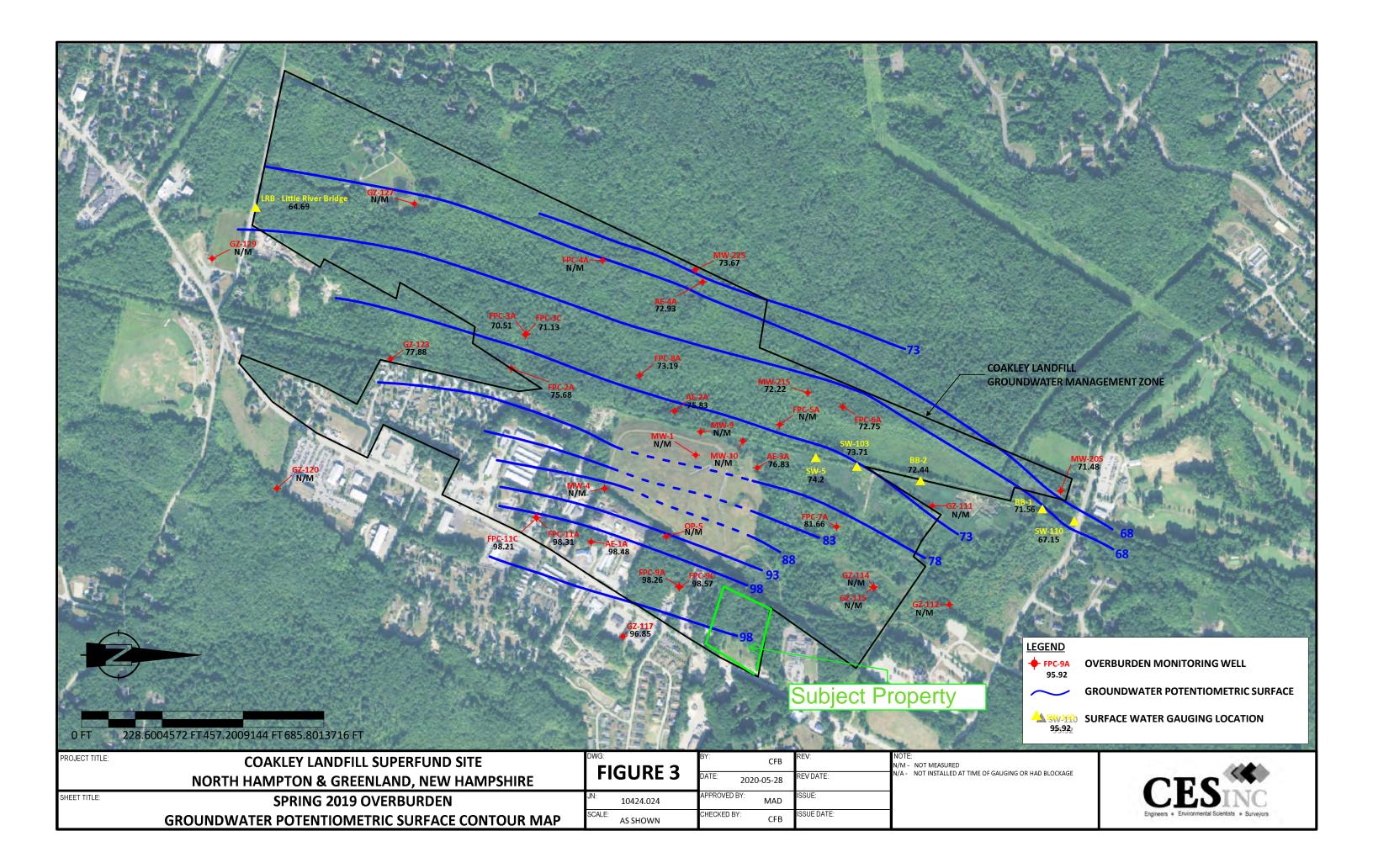
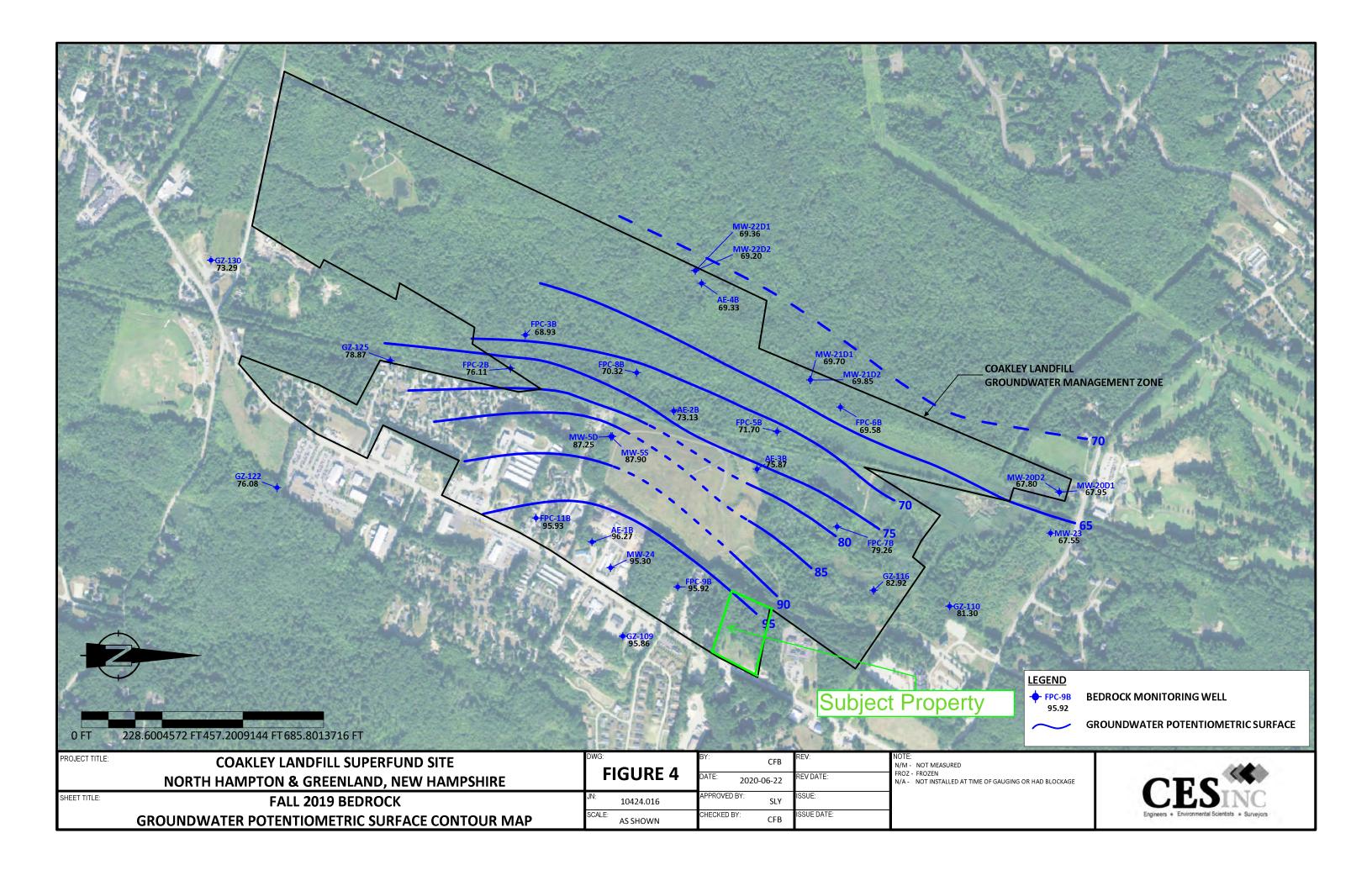
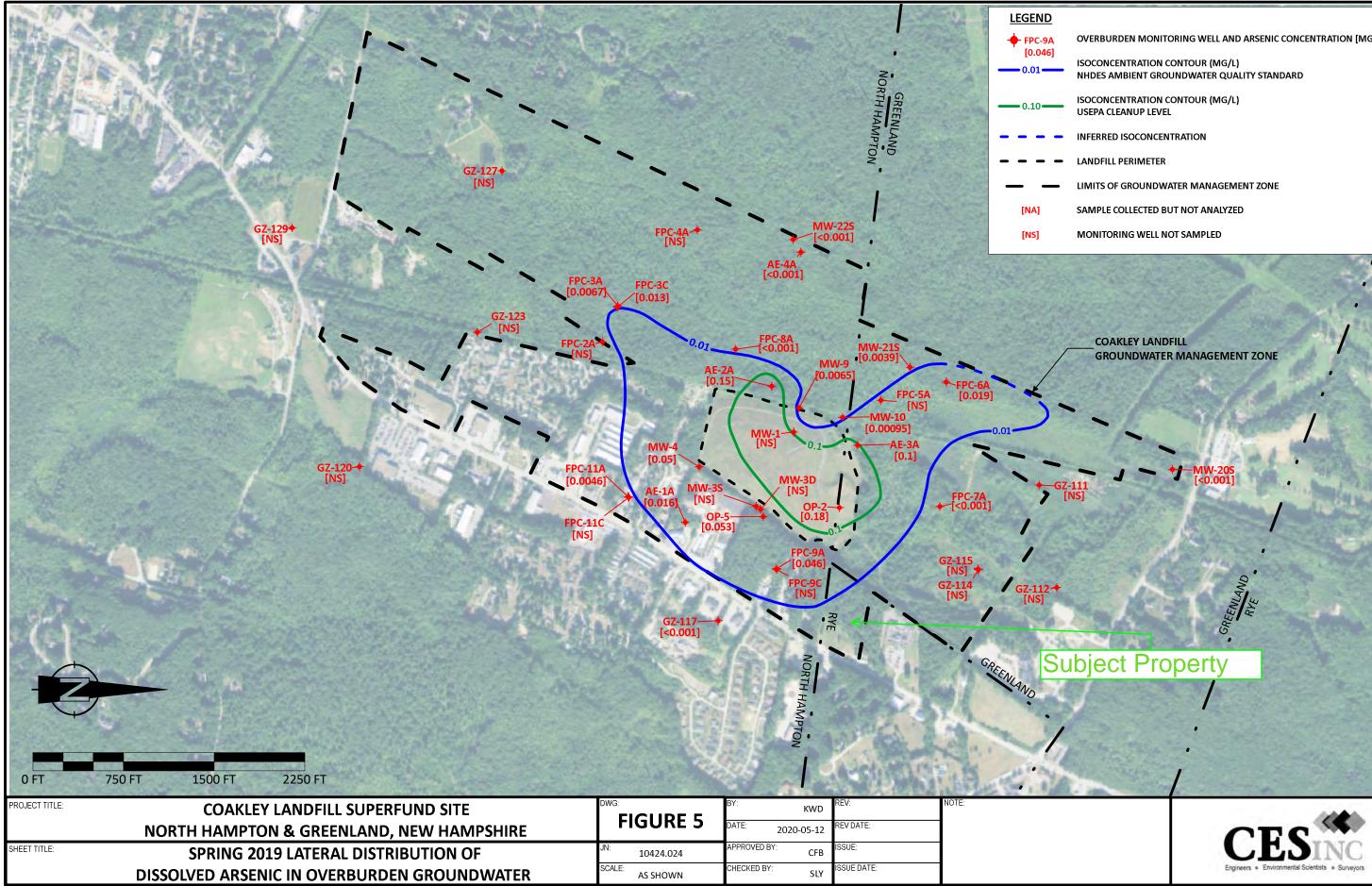


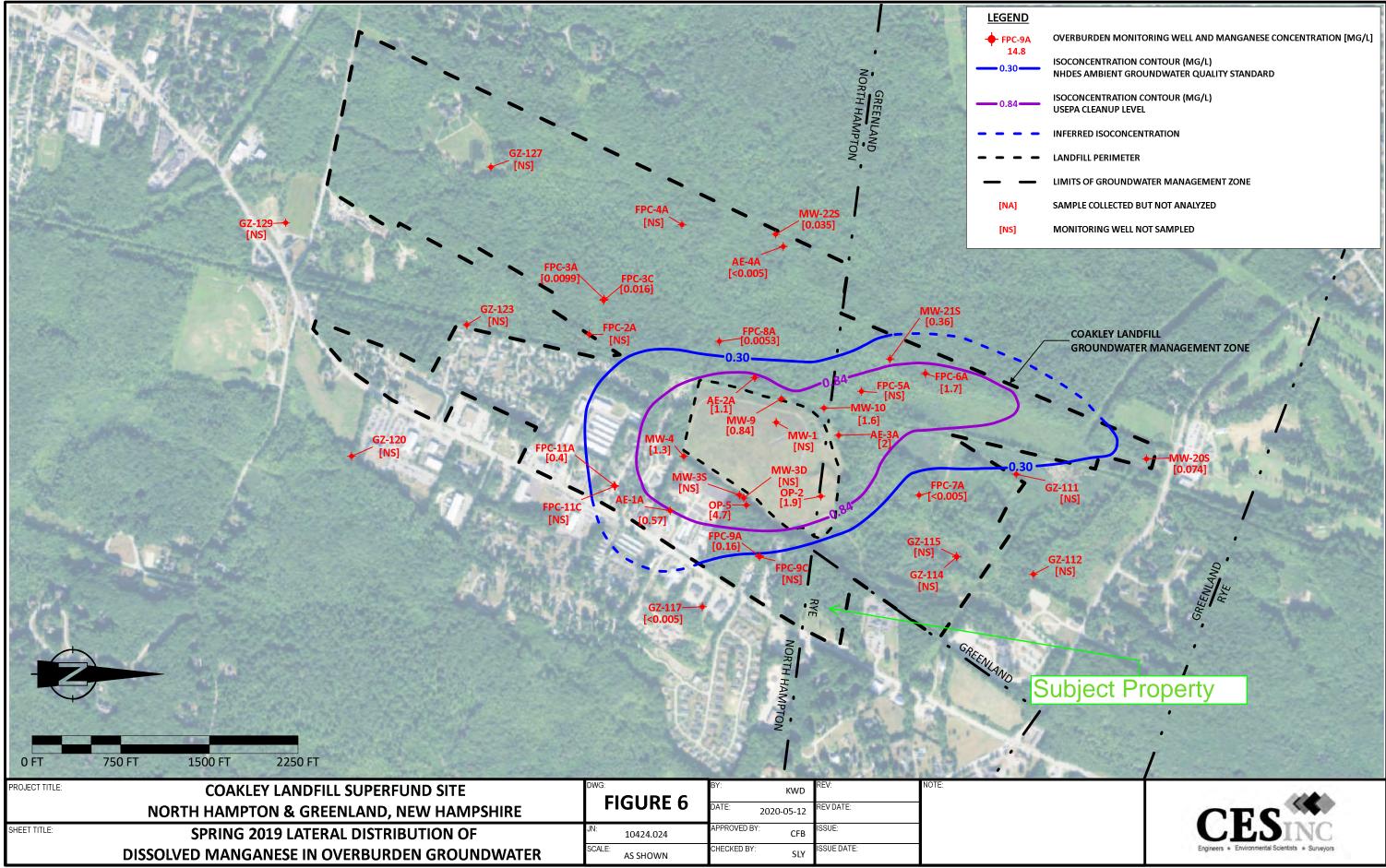
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C			)19-11	1:4,80		OSES		R4 R3						IC F Sta	TO	F.207-969-4881	P.207-200-0000	P.207-790-0120	F.207-255-6307
Π	10424.	ROVED B				<u>S</u>	~ –	R2					OVERBURDEN AND BEDROCK MONITORING WELLS		NC	Presque Isle 549 Main Street PO Box 827 Presque Isle, ME	Waterville 44 Main Street Suite 204 Waterville, ME	Saco 146 Main Street Suite 300 Saco, ME	BWLK, a division of CES, Inc. 13041 McGregor Bive Fort Myers, FL 33919
Ν	016	MAD					RI	R1 EV. I	DESCRIPTION	DATE	DRAWN BY	CHECKED BY		Engineers   Environmental Scientists	Surveyors	Presque Isle, ME T.207-764-8412 F.207-764-8414	Waterville, ME T.207-680-2202 F.207-680-2204	Sec. ME T.207-283-9151 F.207-283-9136	T.239-481-1331 F.239-481-1073

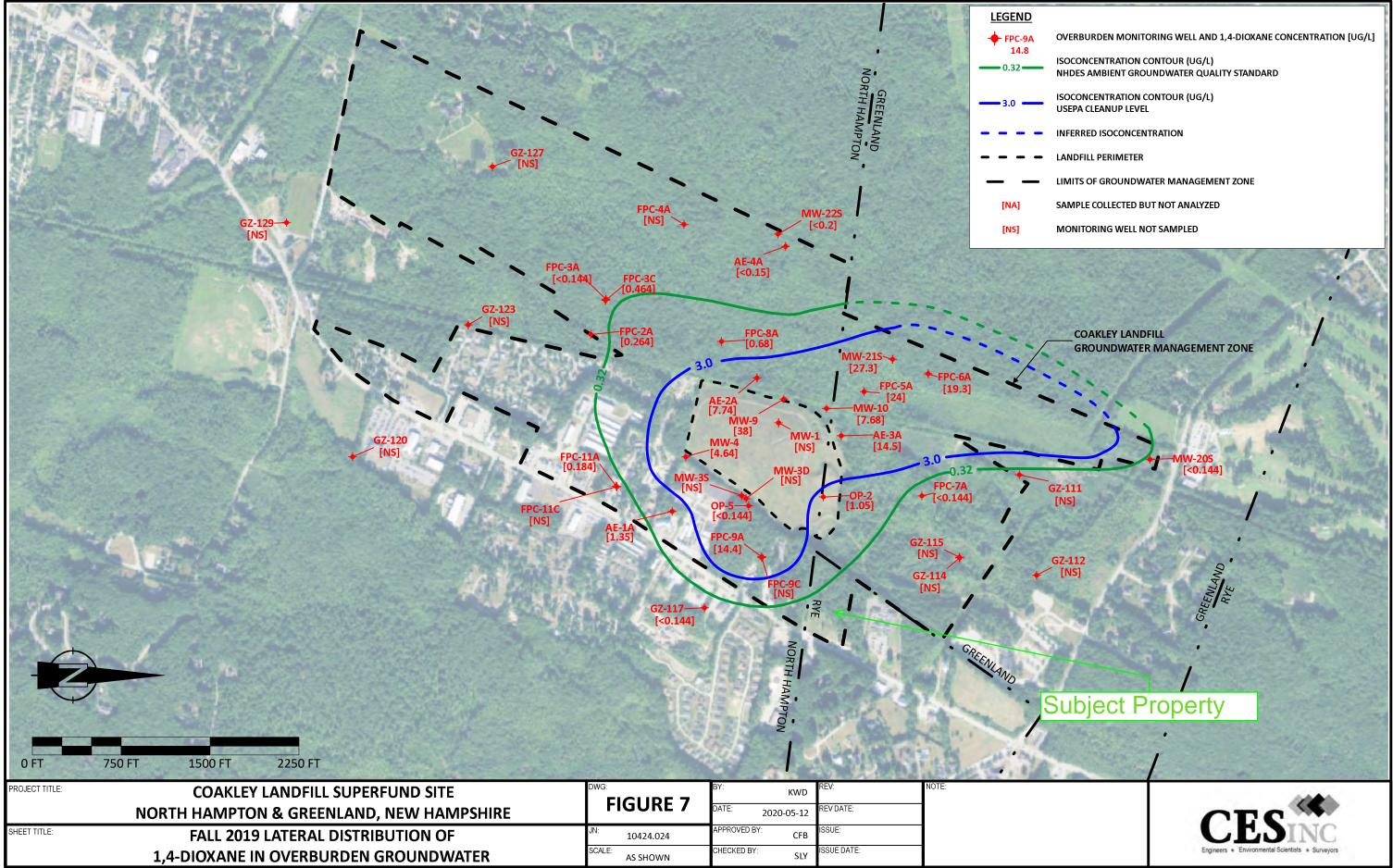


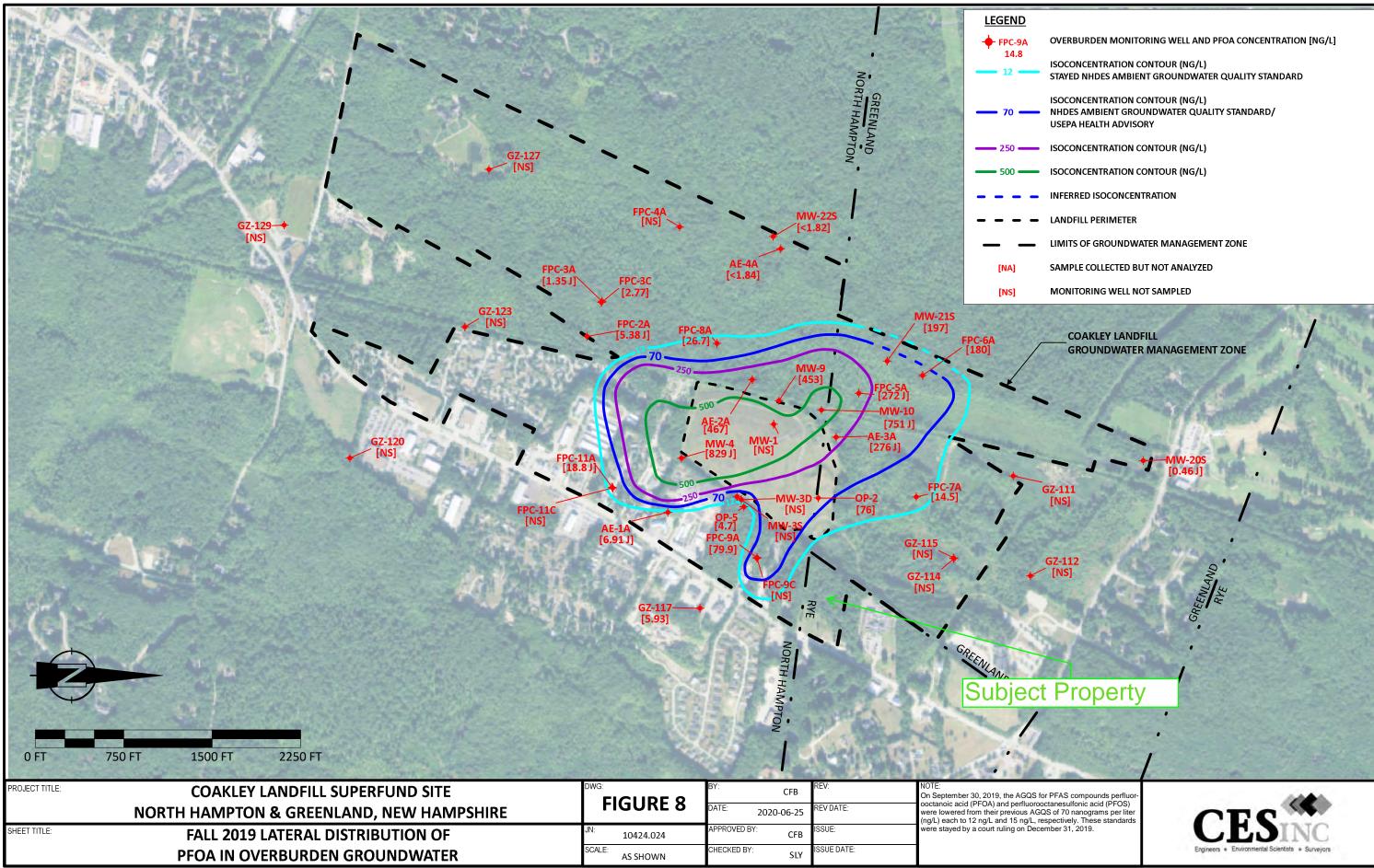


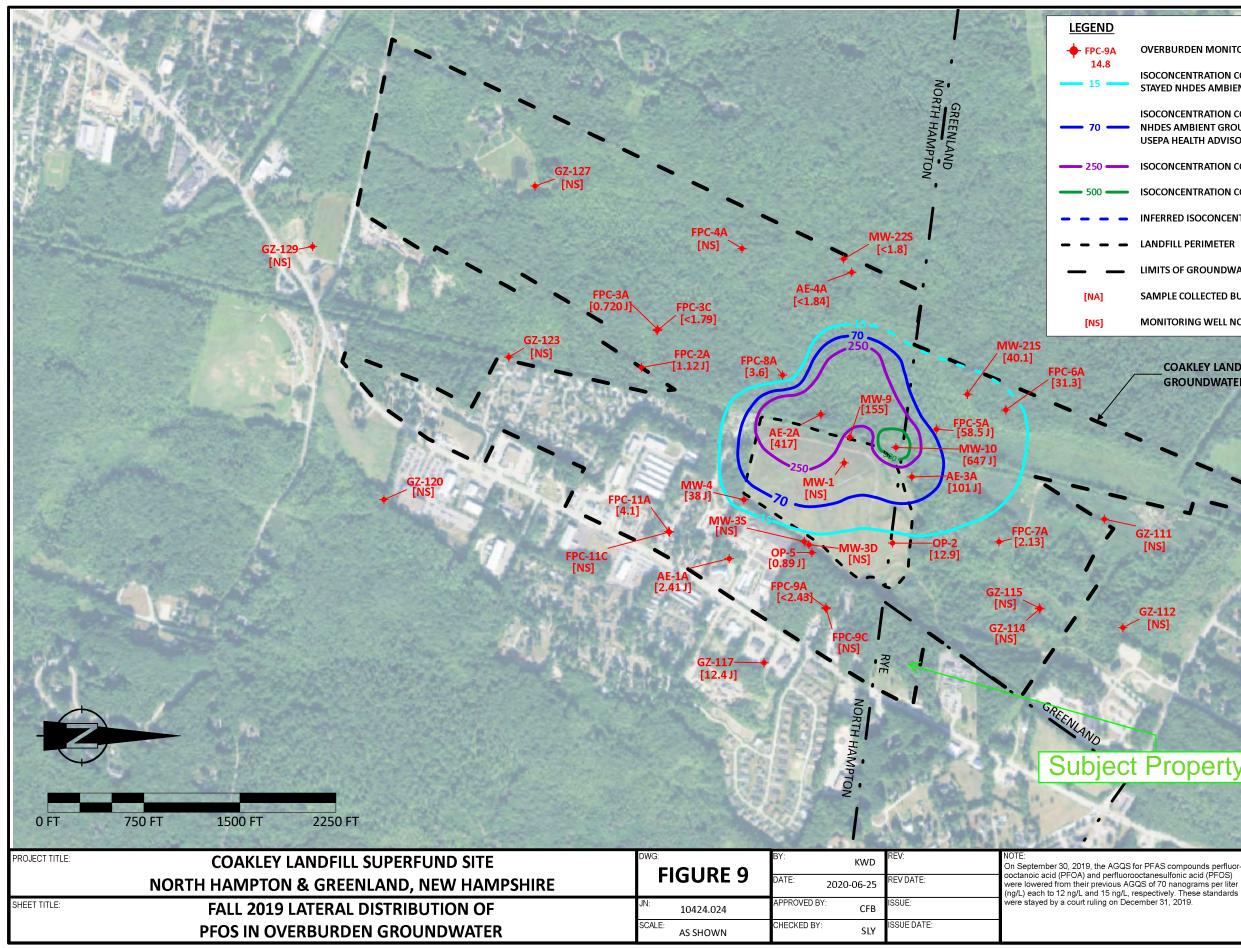


OVERBURDEN MONITORING WELL AND ARSENIC CONCENTRATION [MG/L]









OVERBURDEN MONITORING WELL AND PFOA CONCENTRATION [NG/L]

ISOCONCENTRATION CONTOUR (NG/L) STAYED NHDES AMBIENT GROUNDWATER QUALITY STANDARD

ISOCONCENTRATION CONTOUR (NG/L) NHDES AMBIENT GROUNDWATER QUALITY STANDARD/ USEPA HEALTH ADVISORY

ISOCONCENTRATION CONTOUR (NG/L)

ISOCONCENTRATION CONTOUR (NG/L)

INFERRED ISOCONCENTRATION

LANDFILL PERIMETER

LIMITS OF GROUNDWATER MANAGEMENT ZONE

SAMPLE COLLECTED BUT NOT ANALYZED

MONITORING WELL NOT SAMPLED



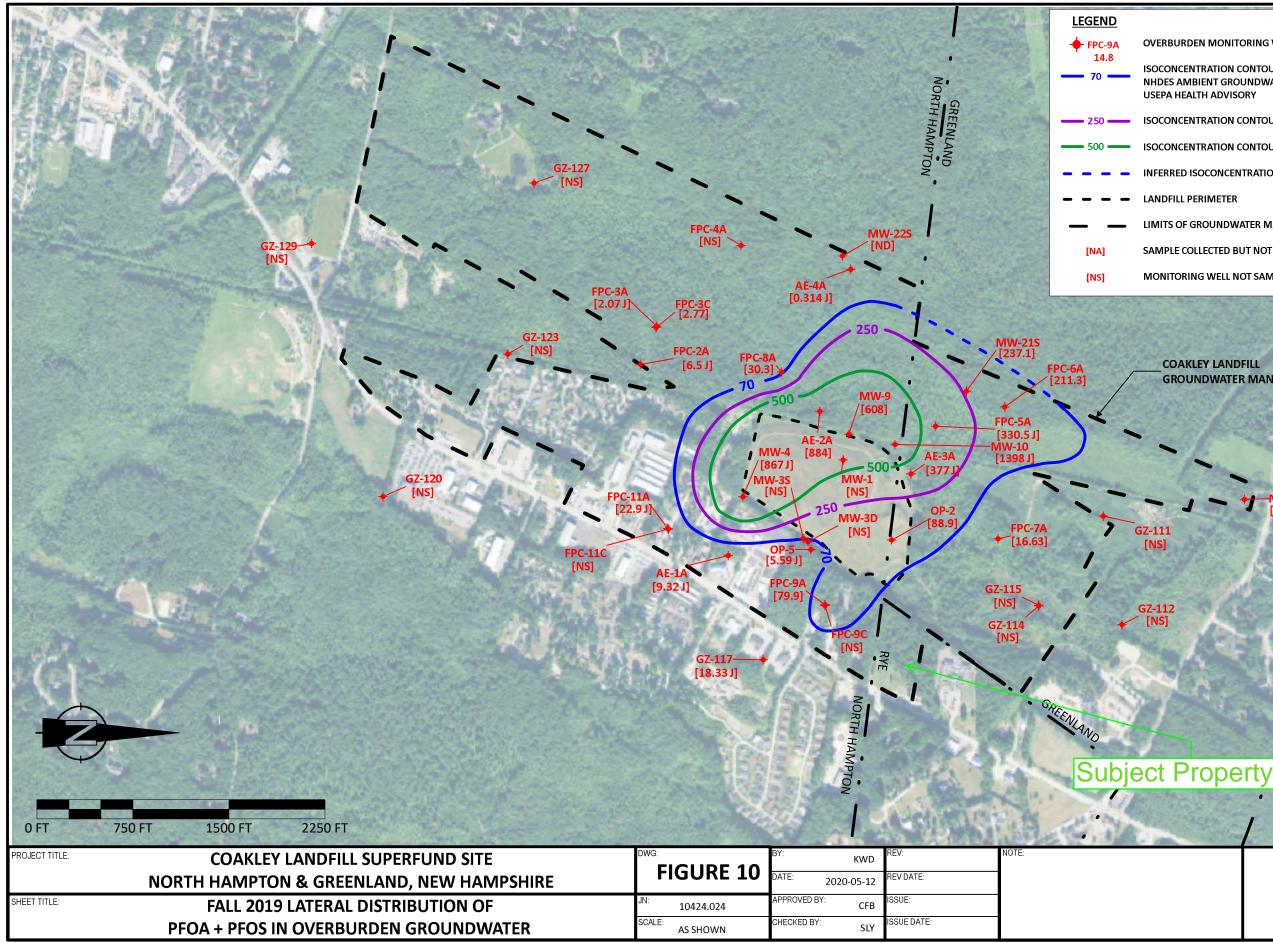
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GZ-112 [NS]

[NS]







OVERBURDEN MONITORING WELL AND PFOA/PFOS CONCENTRATION [NG/L]

ISOCONCENTRATION CONTOUR (NG/L) NHDES AMBIENT GROUNDWATER QUALITY STANDARD/ USEPA HEALTH ADVISORY

ISOCONCENTRATION CONTOUR (NG/L)

INFERRED ISOCONCENTRATION

LANDFILL PERIMETER

LIMITS OF GROUNDWATER MANAGEMENT ZONE

SAMPLE COLLECTED BUT NOT ANALYZED

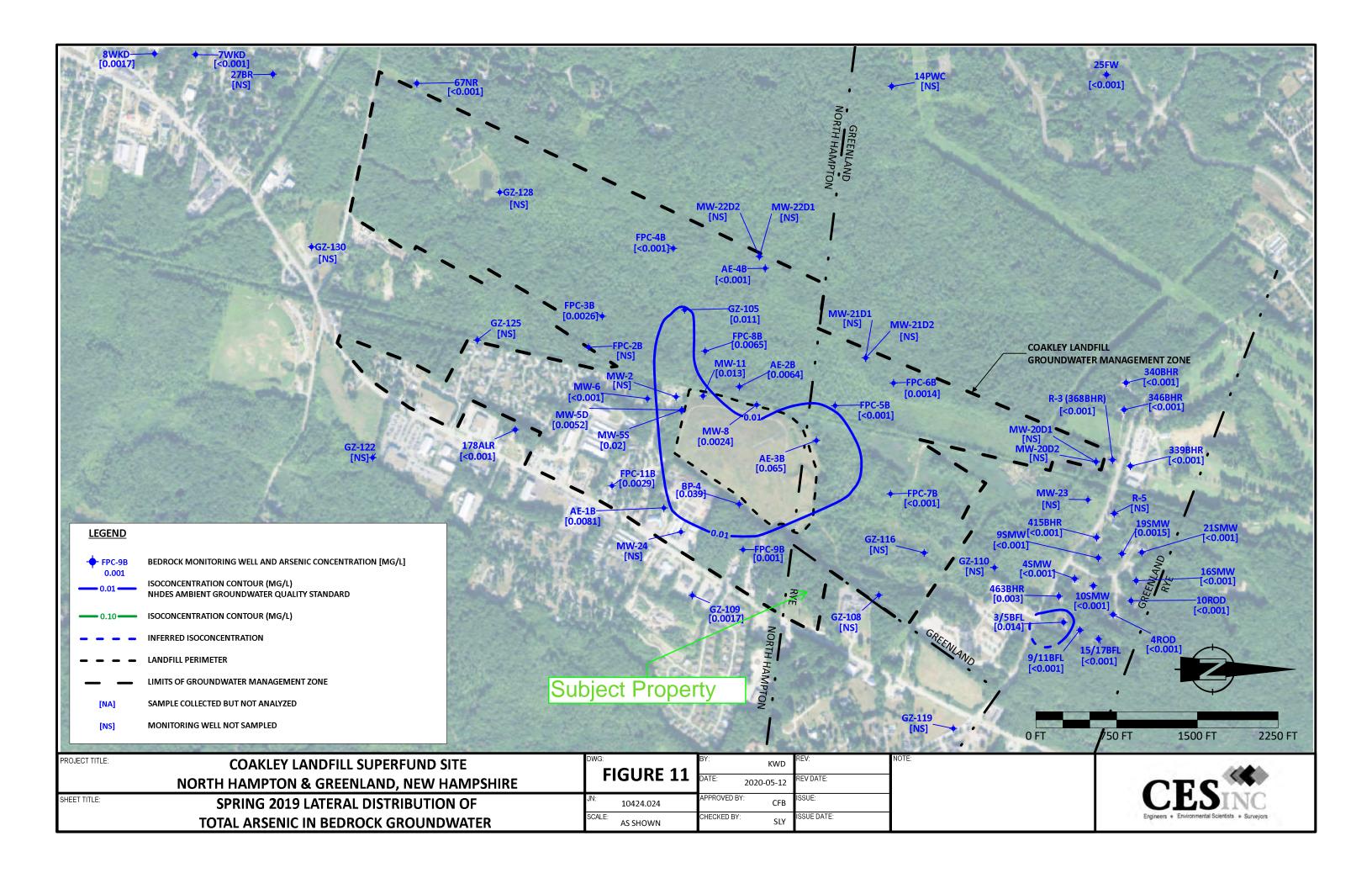
MONITORING WELL NOT SAMPLED

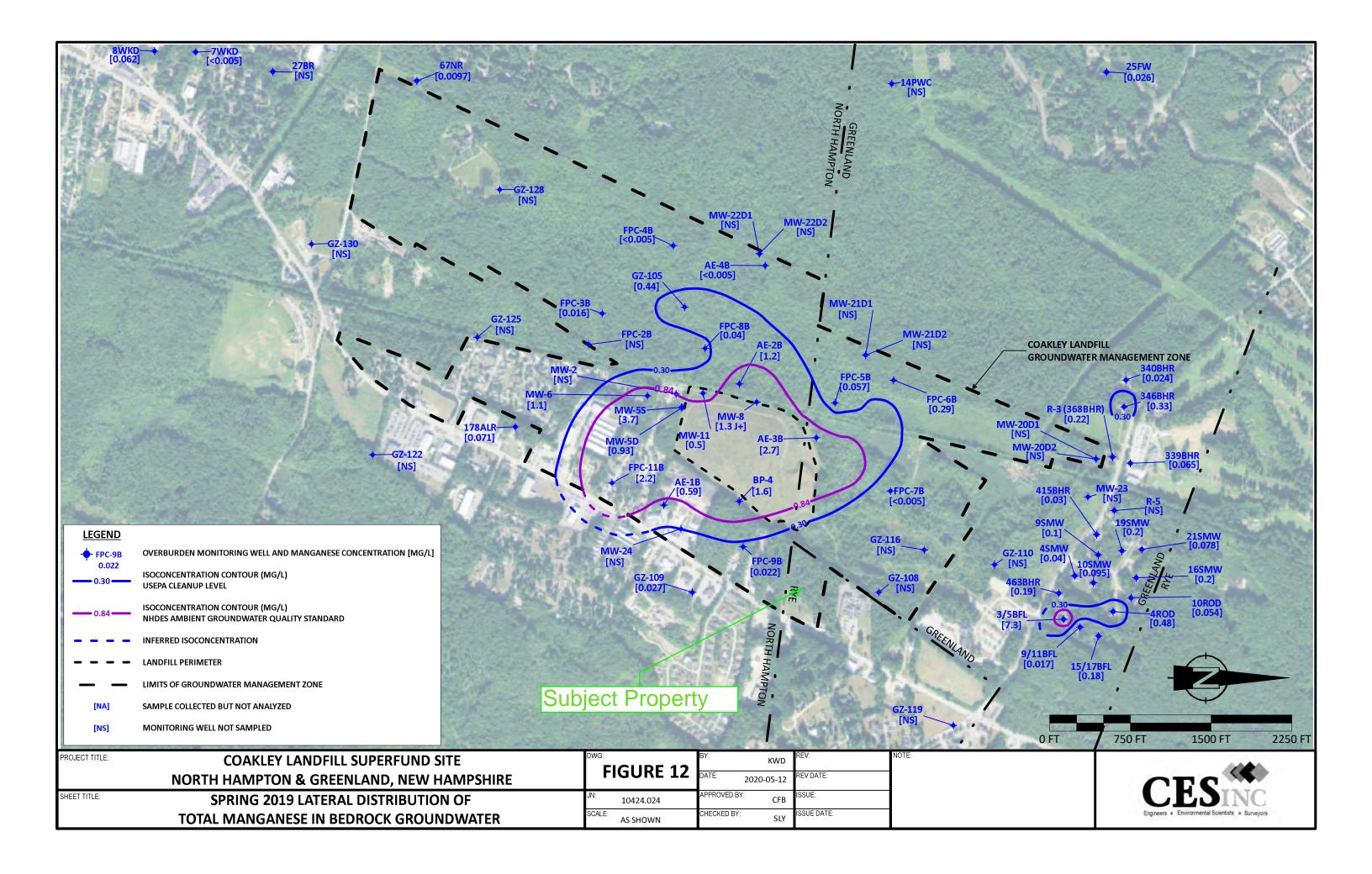
**COAKLEY LANDFILL** GROUNDWATER MANAGEMENT ZONE

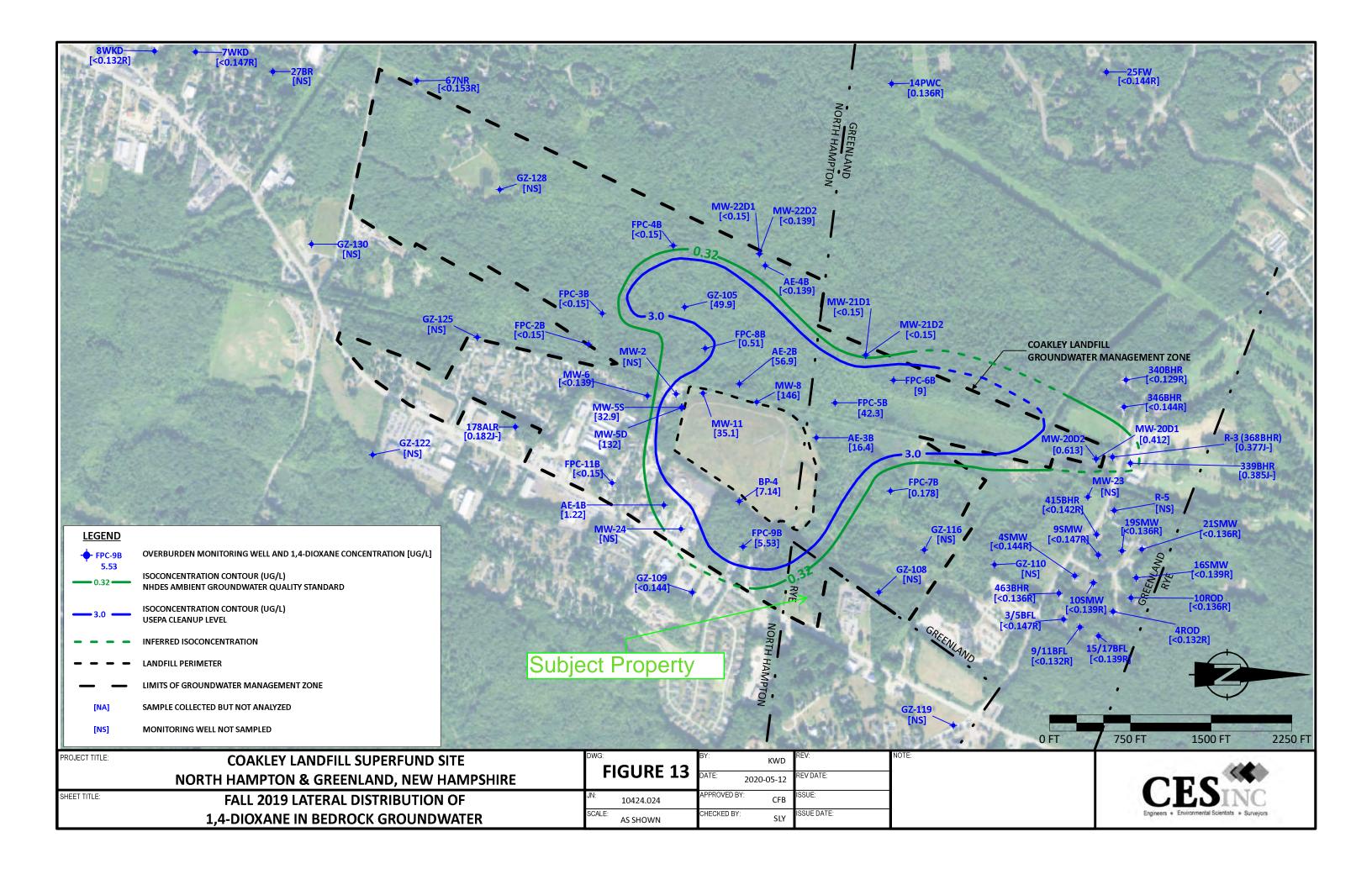
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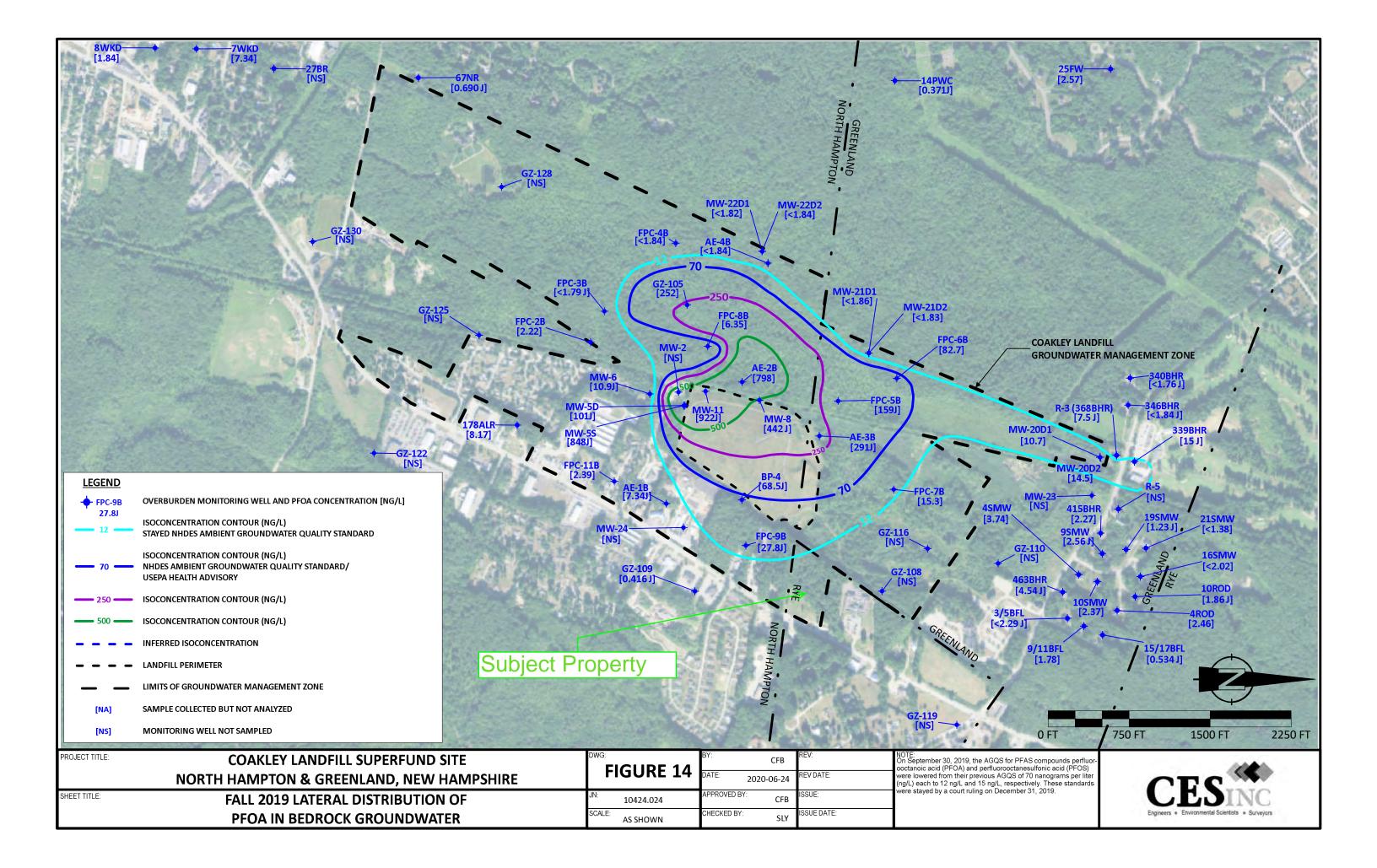


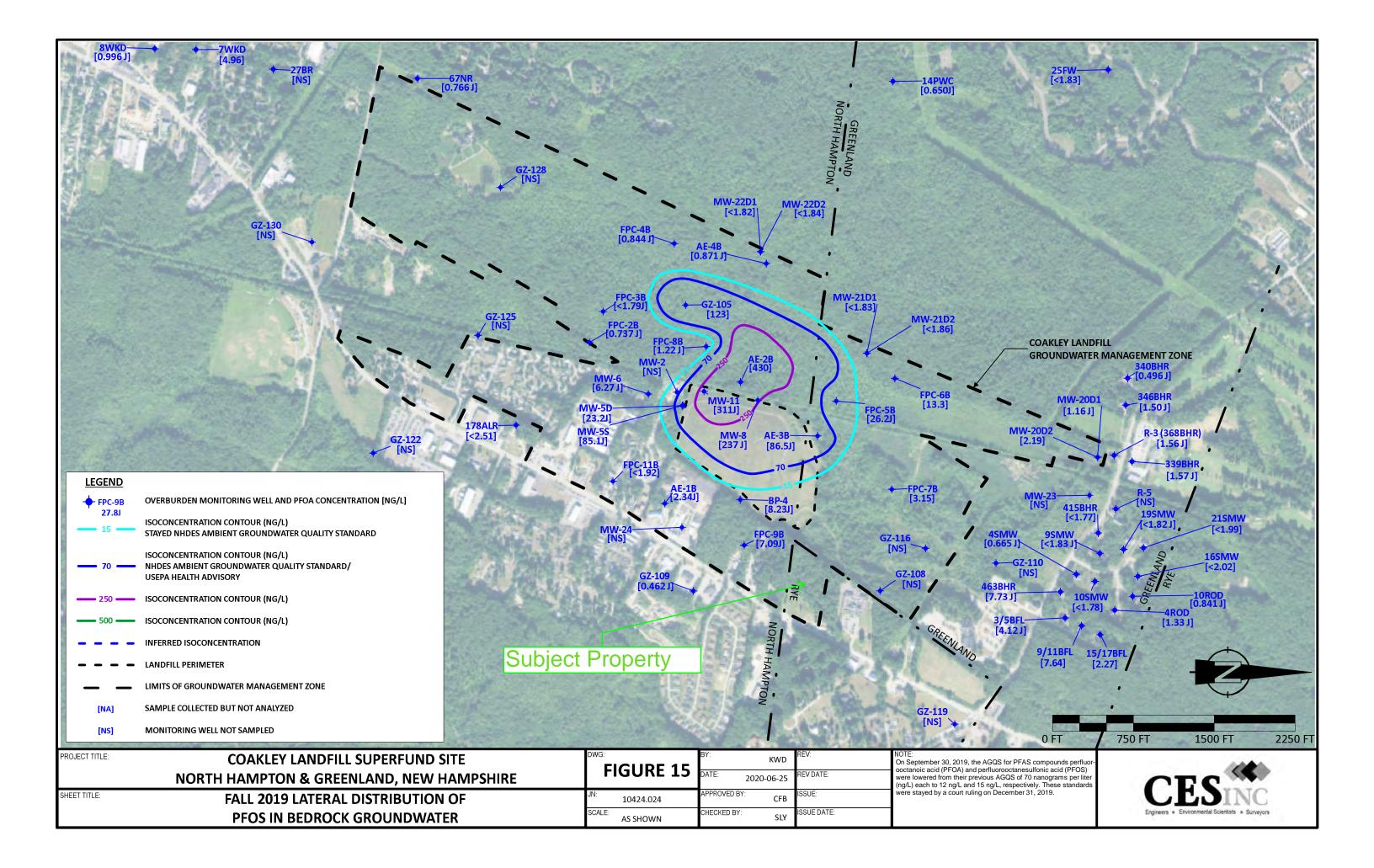
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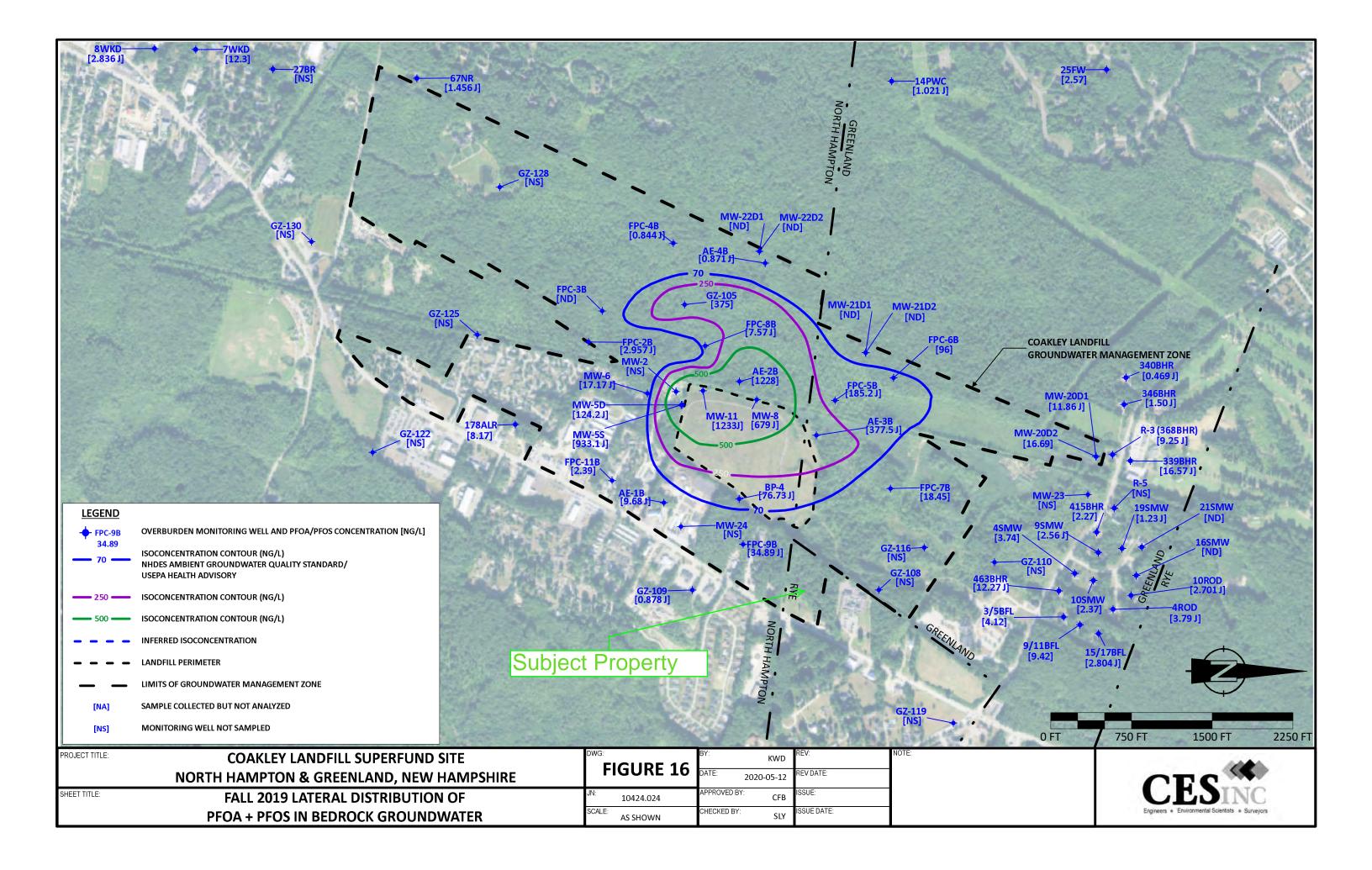












# ATTACHMENT F

# GROUNDWATER MOUNDING AND NITRATE LOADING/MASS BALANCE SPREADSHEETS

PROJECT 9212-007 | June 17, 2021 NEW HAMPSHIRE | MASSACHUSETTS | CONNECTICUT | MAINE GEOINSIGHT.COM | INFO@GEOINSIGHT.COM | 800.271.1953 Maximum groundwater mound height in response to uniform percolation given by Hantush (1967) is:

 $h_{m}^{2}-h_{i}^{2}=(2\omega/K)vtS^{*}(\alpha,\beta)$ 

Where:

h<sub>m</sub> = maximum saturated thickness as a result of loading (ft)

- $h_i$  = initial saturated thickness (ft)
- $$\begin{split} \omega &= \text{loading rate (cubic feet per day)} \\ \text{or } (Q/7.4805)/(2l^* 2a) \\ Q &= \text{loading rate (GPD)} \\ l &= \text{half length of loading area (ft)} \\ \alpha &= \text{half width of loading area (ft)} \\ \text{K} &= \text{hydraulic conductivity (ft/day)} \\ \nu &= \text{Kb/}\epsilon \\ b &= \frac{1}{2}(h_i + h_m) \approx h_i \text{ since } (h_i h_m) \ll h_i \\ \epsilon &= \text{ porosity (dimensionless)} \\ \text{t} &= \text{duration of loading (days)} \\ \text{S}^*(\alpha,\beta) &= \text{ an integral error function determined from tables} \\ \alpha &= \frac{l}{(4 \vee t)^{\frac{1}{2}}} \end{split}$$
  - $\beta = a / (4vt)^{\frac{1}{2}}$

Given:

h	=	10	ft
Κ	=	23	ft/day
3	=	0.2	
2l	=	42	ft
<b>2</b> <i>a</i>	=	16.5	ft
Q	=	960	GPD
t	=	30.0	days

Solution:

```
960 / 7.4805 ) / ( 42 * 16.5 ) = 0.19
\omega = (
v = (23 * 10) / 0.2 = 1150.00
                             (30.0)^{\frac{1}{2}} = 0.057
\alpha = (21) / (4 * 1150) *
                             (30.0)^{\frac{1}{2}} = 0.022
\beta = (8.25 / (4 * 1150 * 
S^{*}(\alpha,\beta) = 0.0101 (from table)
h_m^2 - h_i^2 = (2 *
                 0.19
                       / 23 )* 1150.0 * 30.00 * 0.0101 = 5.61
                       (10^{2})^{\frac{1}{2}} =
          5.61
                                    10.28
h_m = (
                  +
Mound Height = 10.28 - h_i =
                                     0.3
                                           feet
```

Maximum groundwater mound height in response to uniform percolation given by Hantush (1967) is:

 $h_{m}^{2}-h_{i}^{2}=(2\omega/K)vtS^{*}(\alpha,\beta)$ 

Where:

h<sub>m</sub> = maximum saturated thickness as a result of loading (ft)

 $h_i$  = initial saturated thickness (ft)

$$\begin{split} \omega &= \text{loading rate (cubic feet per day)} \\ \text{or } (Q/7.4805)/(2l^* 2a) \\ Q &= \text{loading rate (GPD)} \\ l &= \text{ half length of loading area (ft)} \\ \alpha &= \text{ half width of loading area (ft)} \\ \text{K} &= \text{hydraulic conductivity (ft/day)} \\ \text{v} &= \text{Kb/}\epsilon \\ \text{b} &= \frac{1}{2}(h_i + h_m) \approx h_i \text{ since } (h_i - h_m) \ast h_i \\ \epsilon &= \text{ porosity (dimensionless)} \\ \text{t} &= \text{ duration of loading (days)} \\ \text{S}^*(\alpha,\beta) &= \text{ an integral error function determined from tables} \\ \alpha &= \frac{1}{(4vt)^{\frac{1}{2}}} \\ \beta &= \frac{\alpha}{(4vt)^{\frac{1}{2}}} \end{split}$$

Given:

h <sub>i</sub>	=	10	ft
Κ	=	23	ft/day
З	=	0.2	
2l	=	42	ft
<b>2</b> <i>a</i>	=	16.5	ft
Q	=	960	GPD
t	=	180.0	days

Solution:

```
\begin{split} & \omega = ( 960 / 7.4805 ) / ( 42 * 16.5 ) = 0.19 \\ & v = ( 23 * 10 ) / 0.2 = 1150.00 \\ & \alpha = ( 21 / (4 * 1150 * 180.0 )^{\frac{1}{2}} = 0.023 \\ & \beta = ( 8.25 / (4 * 1150 * 180.0 )^{\frac{1}{2}} = 0.009 \\ & S^*(\alpha,\beta) = 0.0041 \quad (\text{from table}) \\ & h_m^2 - h_i^2 = (2 * 0.19 / 23 ) * 1150.0 * 180.00 * 0.0041 = 13.67 \\ & h_m = ( 13.67 + 10^2)^{\frac{1}{2}} = 10.66 \\ & \text{Mound Height} = 10.66 - h_i = 0.7 \quad \text{feet} \end{split}
```

Maximum groundwater mound height in response to uniform percolation given by Hantush (1967) is:

 $h_{m}^{2}-h_{i}^{2}=(2\omega/K)vtS^{*}(\alpha,\beta)$ 

Where:

h<sub>m</sub> = maximum saturated thickness as a result of loading (ft)

- h<sub>i</sub> = initial saturated thickness (ft)
- ω = loading rate (cubic feet per day)or (Q/7.4805)/(2*l*\* 2*a*) Q= loading rate (GPD) *l*= half length of loading area (ft) *α*= half width of loading area (ft) K = hydraulic conductivity (ft/day) v = Kb/ε b= ½(h<sub>i</sub>+h<sub>m</sub>) ≈ h<sub>i</sub> since (h<sub>i</sub>-h<sub>m</sub>)«h<sub>i</sub> ε= porosity (dimensionless) t = duration of loading (days) S\*(α,β)= an integral error function determined from tables *α*= *l*/(4vt)<sup>½</sup> β= *a*/(4vt)<sup>½</sup>

Given:

h <sub>i</sub>	=	10	ft
Κ	=	23	ft/day
3	=	0.2	
2 <i>l</i>	=	42	ft
<b>2</b> <i>a</i>	=	16.5	ft
Q	=	960	GPD
t	=	365.0	days

Solution:

```
\begin{split} & \omega = ( 960 / 7.4805 ) / ( 42 * 16.5 ) = 0.19 \\ & v = ( 23 * 10 ) / 0.2 = 1150.00 \\ & \alpha = ( 21 / (4 * 1150 * 365.0 )^{\frac{1}{2}} = 0.016 \\ & \beta = ( 8.25 / (4 * 1150 * 365.0 )^{\frac{1}{2}} = 0.006 \\ & S^*(\alpha,\beta) = 0.0041 \quad (\text{from table}) \\ & h_m^{-2} h_i^{-2} = (2 * 0.19 / 23 ) * 1150.0 * 365.00 * 0.0041 = 27.71 \\ & h_m = ( 27.71 + 10^{-2})^{\frac{1}{2}} = 11.30 \\ & \text{Mound Height} = 11.30 - h_i = 1.3 \quad \text{feet} \end{split}
```

